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Aronson et al.

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(54) **LIGHT REDIRECTING FILM AND DISPLAY SYSTEM INCORPORATING SAME**

6/0053 (2013.01); **B32B 2307/40** (2013.01);
G02F 2001/133607 (2013.01)

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(58) **Field of Classification Search**

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G02B 6/0053; **B32B 2307/40**; **G02F 2001/133607**; **G02F 1/133502**; **G02F 2202/36**
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See application file for complete search history.

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(51) **Int. Cl.**

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G02B 5/02 (2006.01)

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(52) **U.S. Cl.**

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Primary Examiner — Thomas A Hollweg

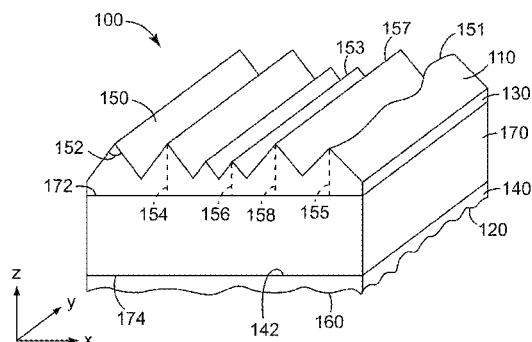
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ABSTRACT

Light redirecting film is disclosed. The light redirecting film includes a first major surface that includes a plurality of first microstructures that extend along a first direction. The light redirecting film also includes a second major surface that is opposite to the first major surface and includes a plurality of second microstructures. The second major surface has an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%. The light redirecting film has an average effective transmission that is not less than about 1.75.

4 Claims, 21 Drawing Sheets



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F21V 8/00
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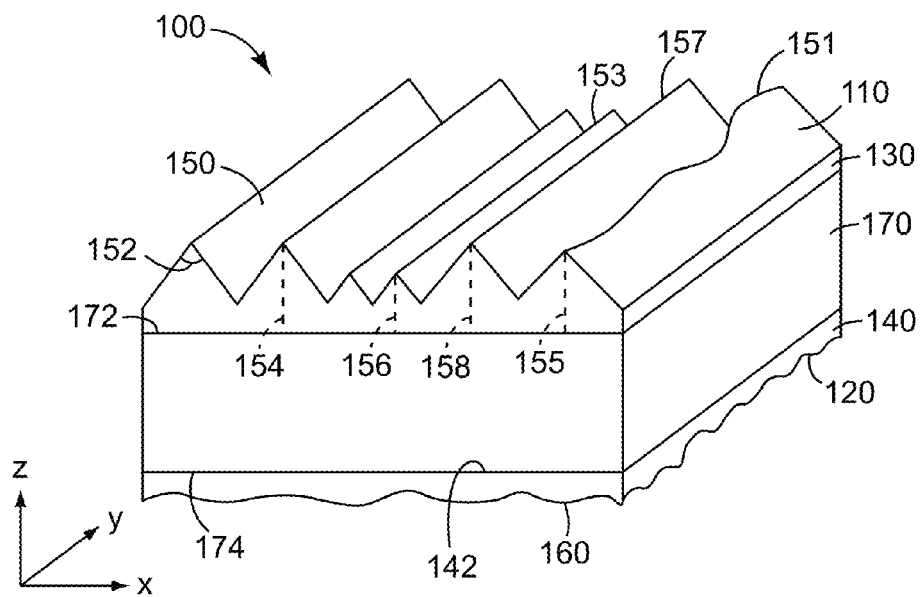


Fig. 1

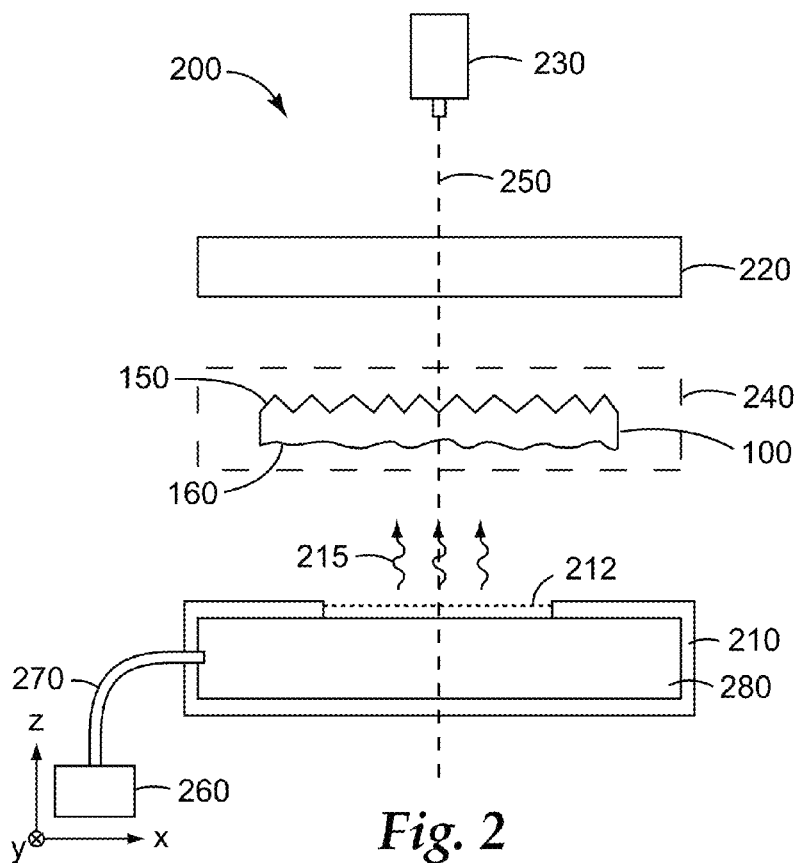
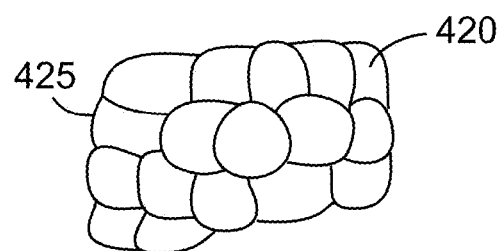
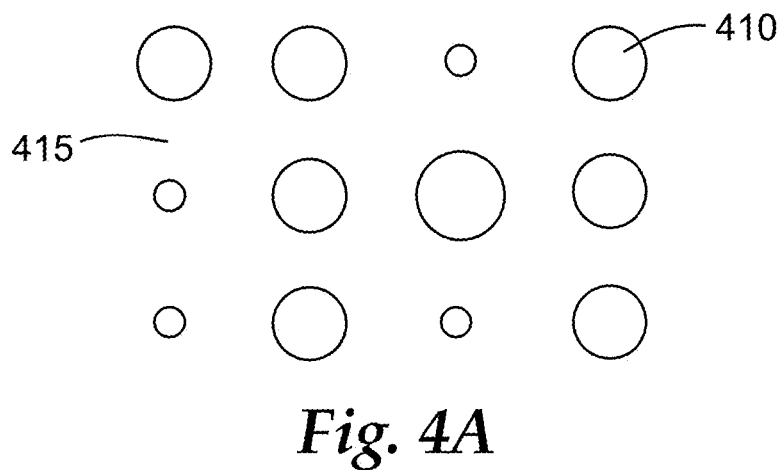
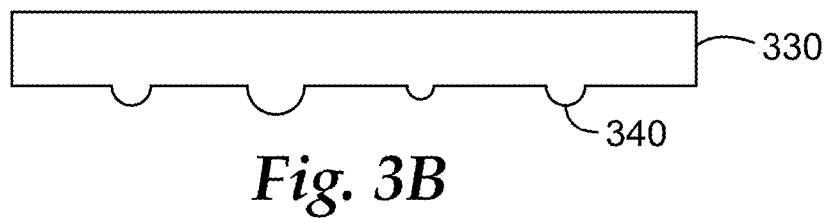
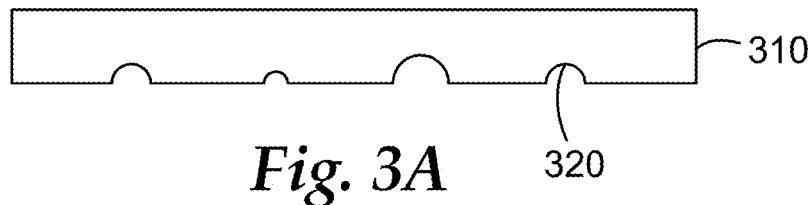


Fig. 2



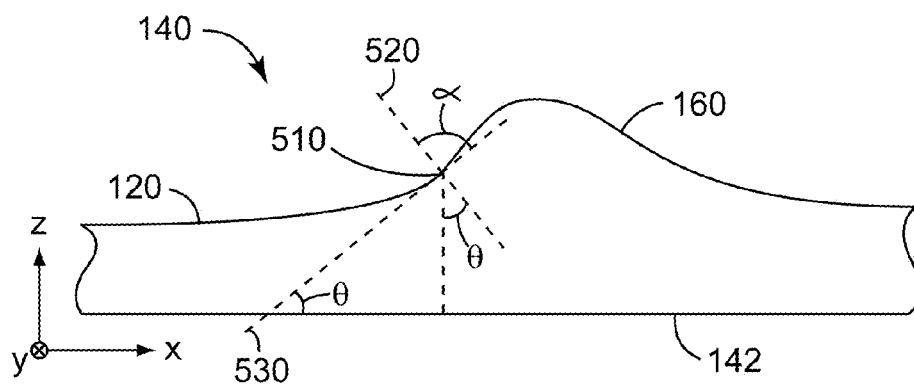


Fig. 5

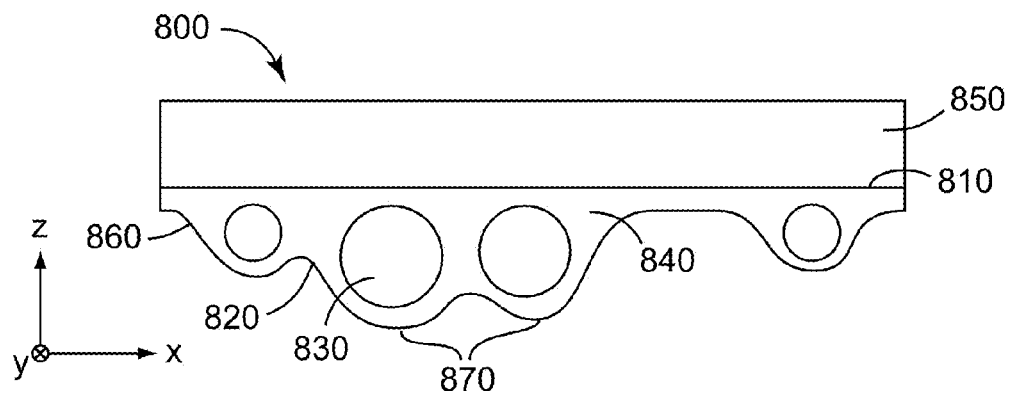


Fig. 8

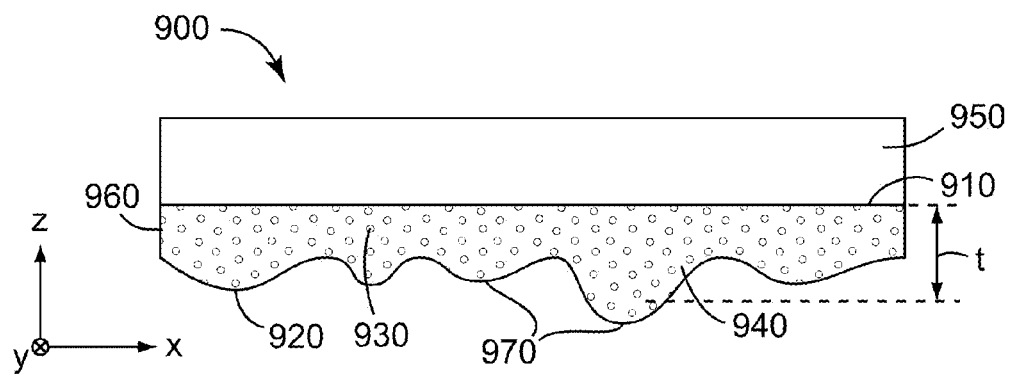


Fig. 9

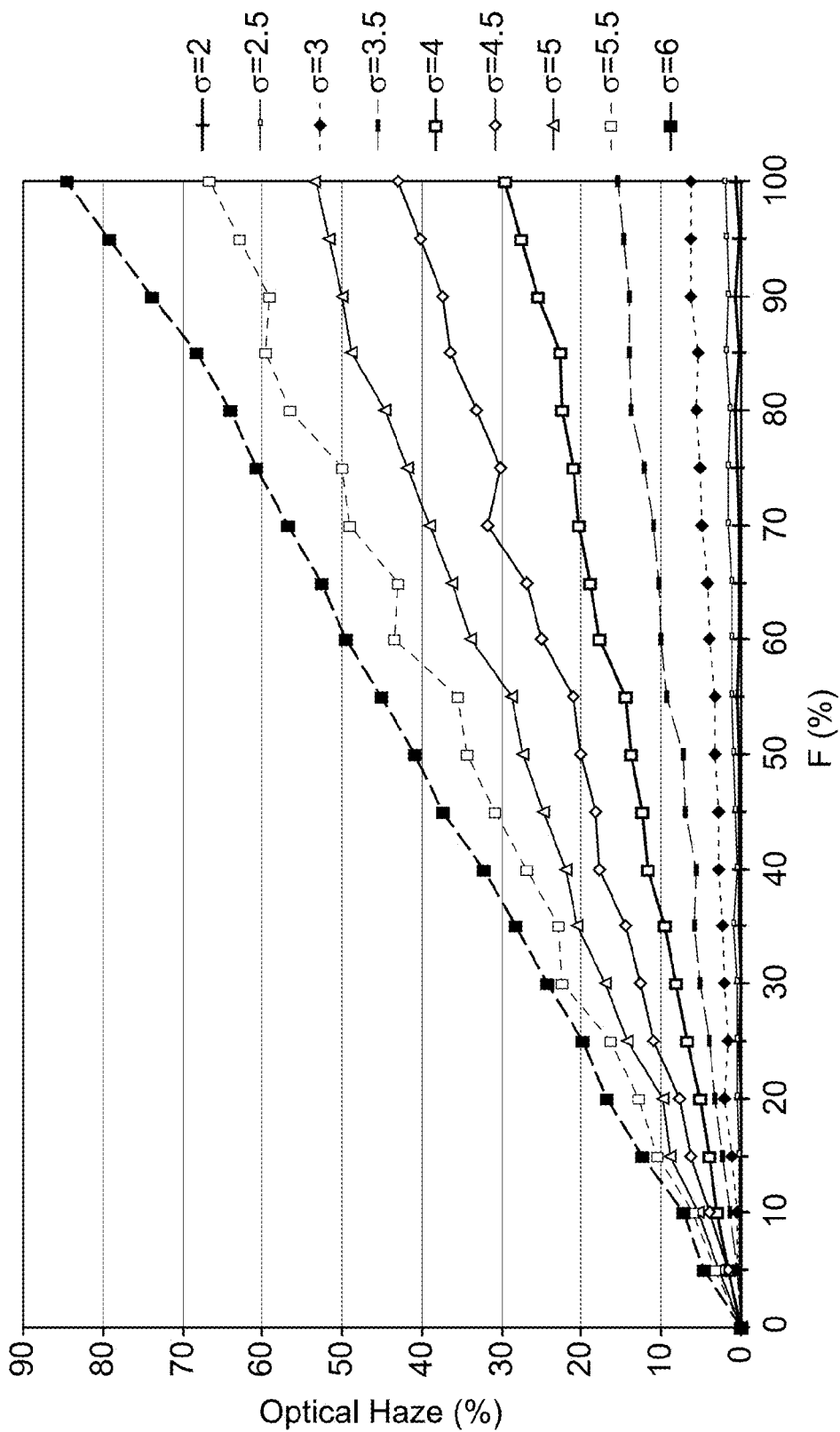


Fig. 6

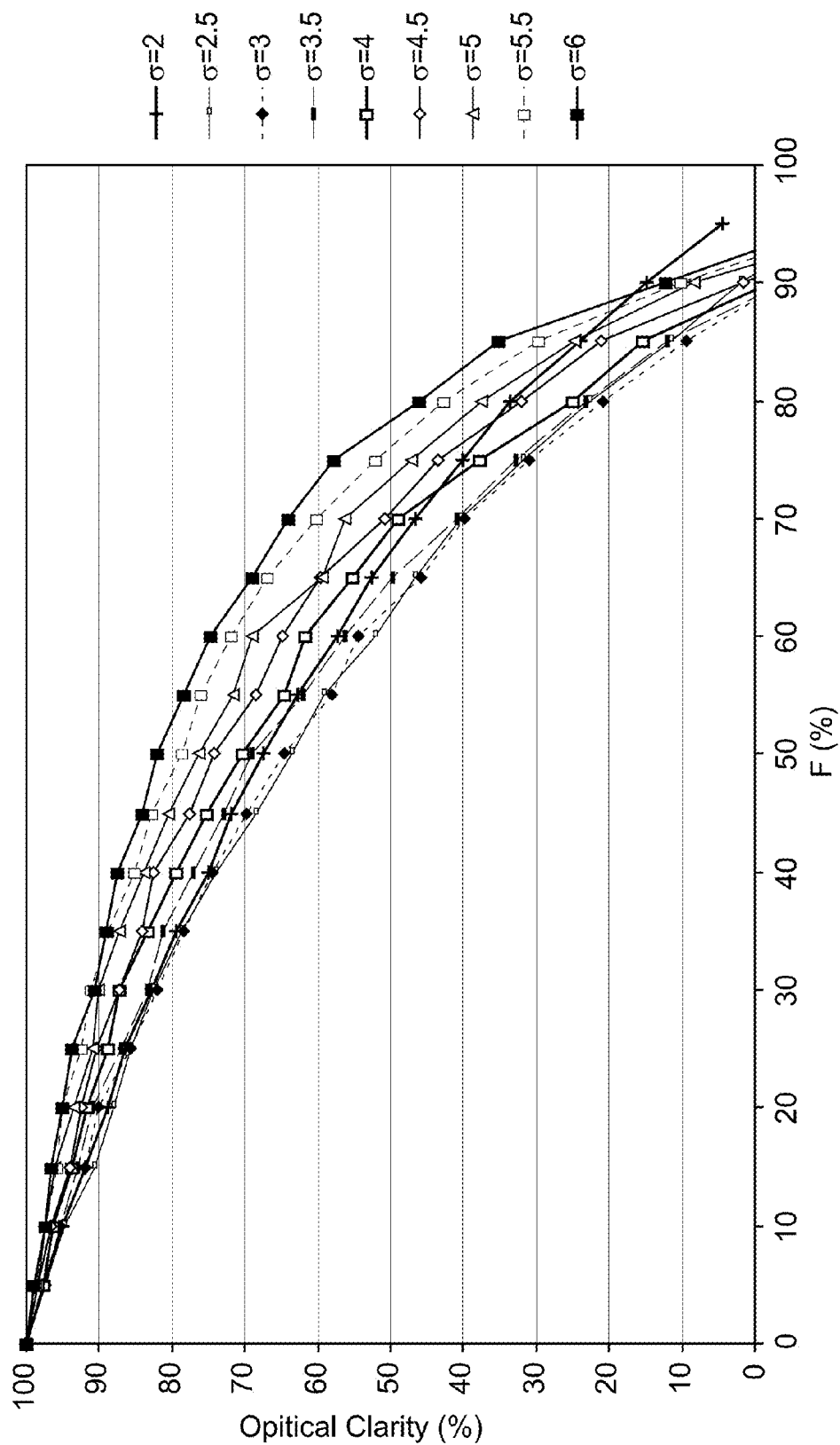


Fig. 7

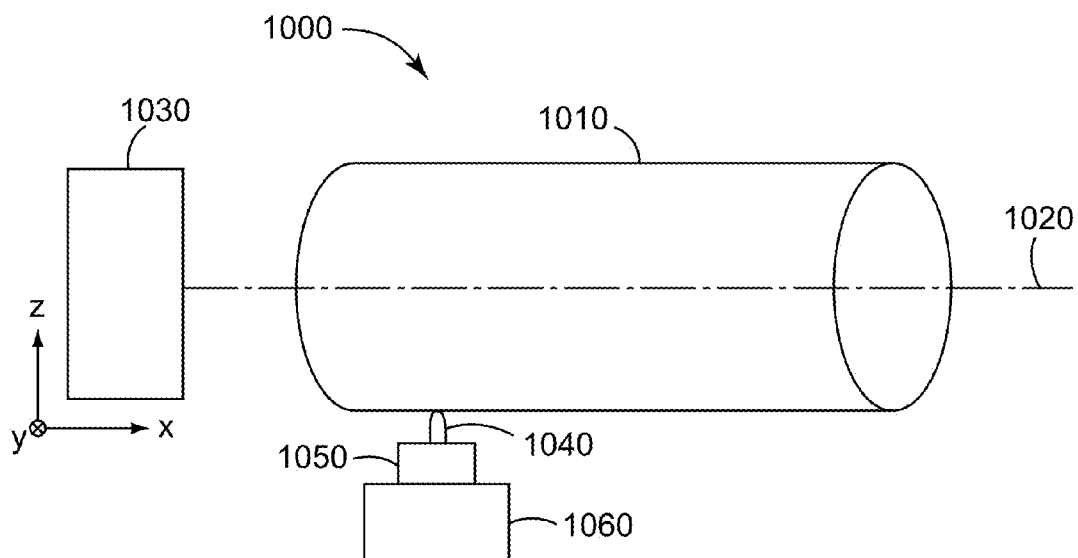


Fig. 10

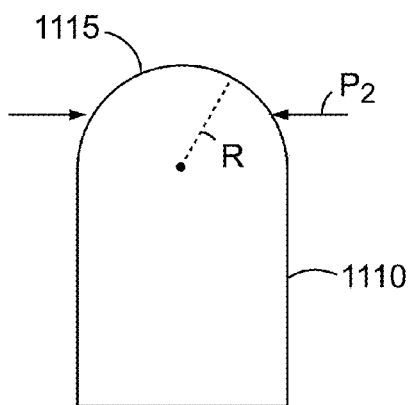


Fig. 11A

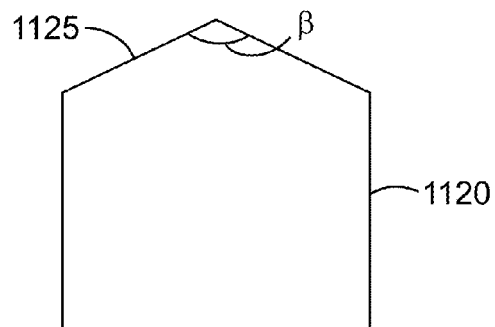


Fig. 11B

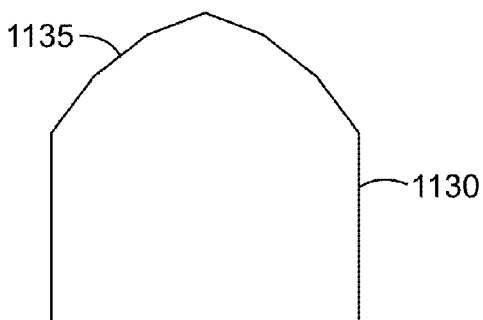


Fig. 11C

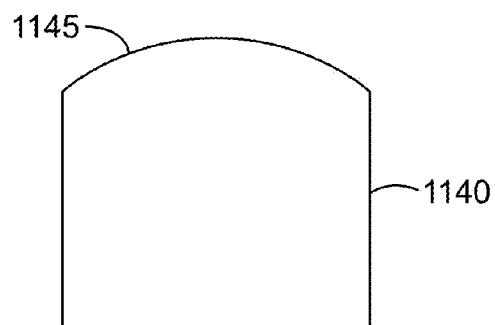
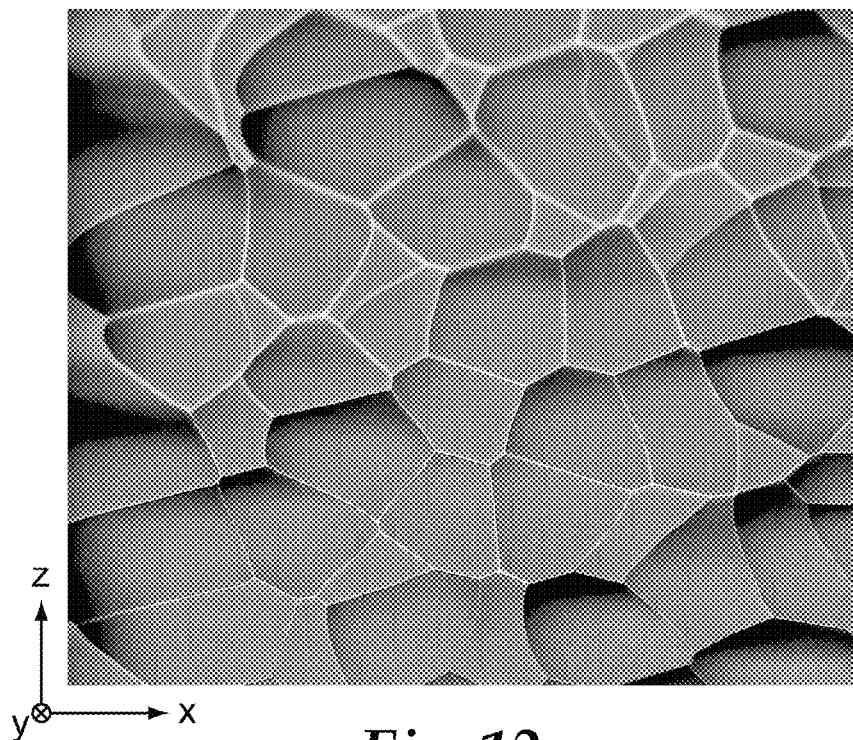
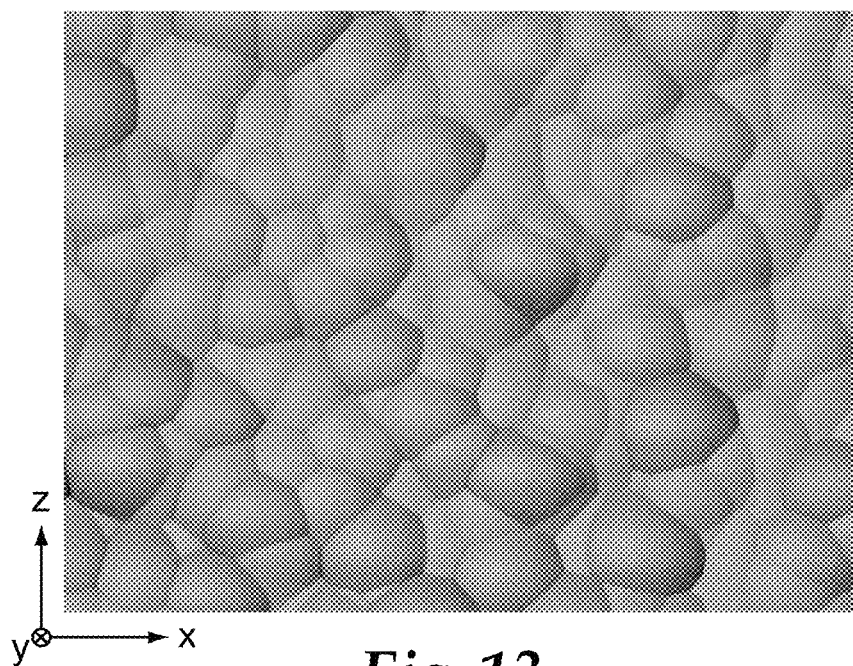
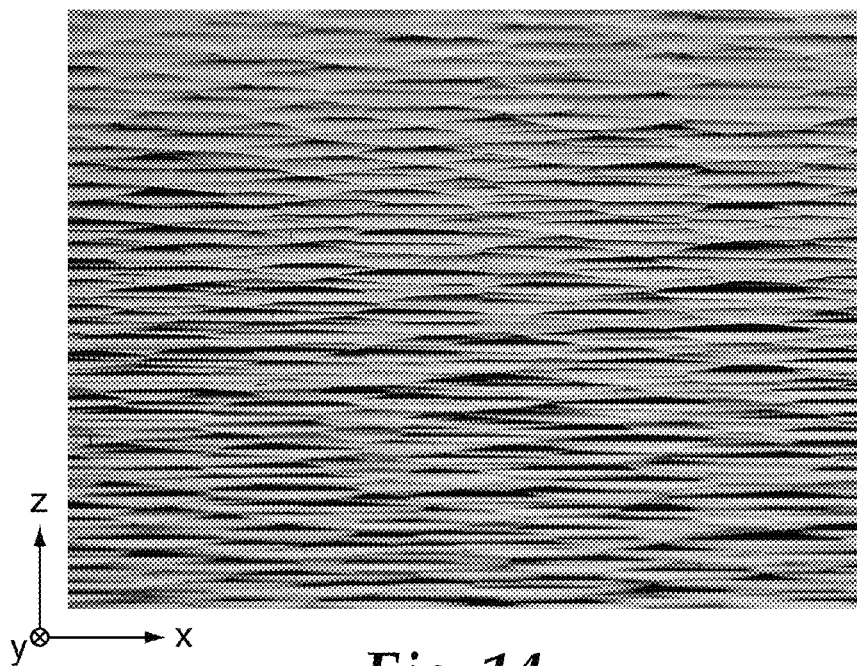
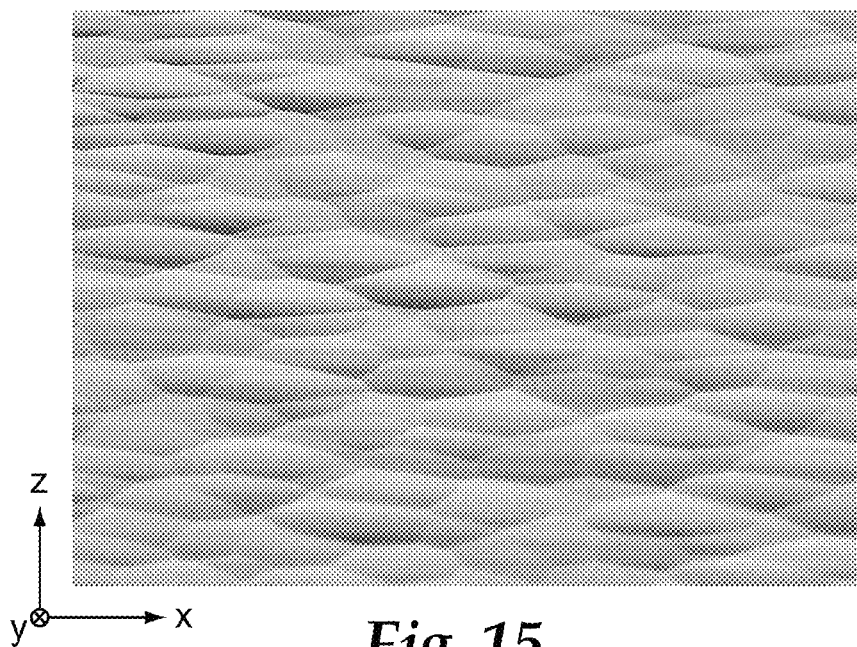
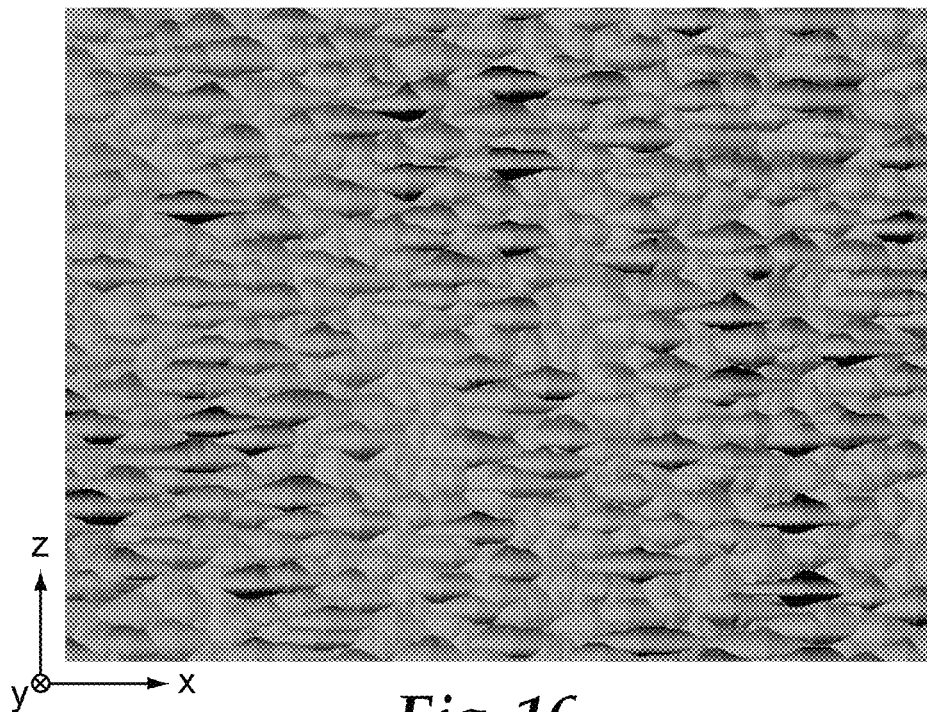
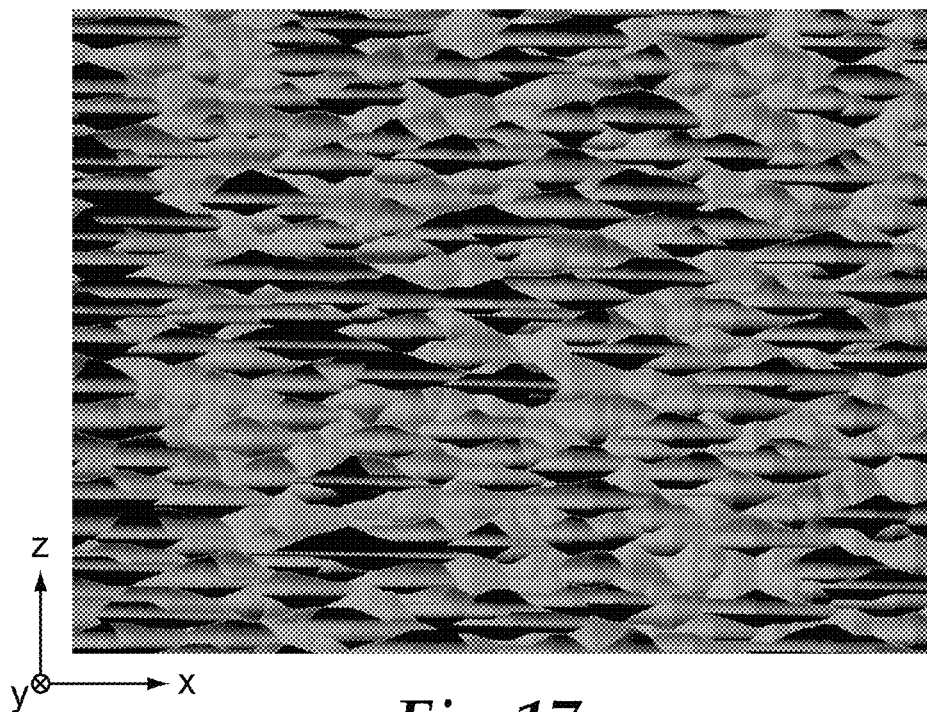
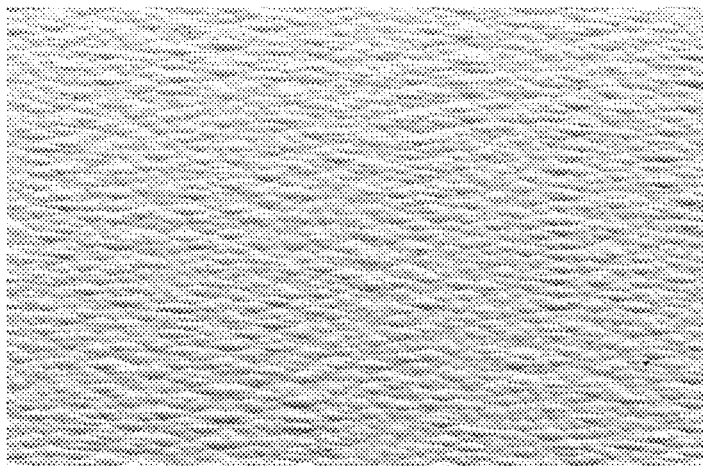
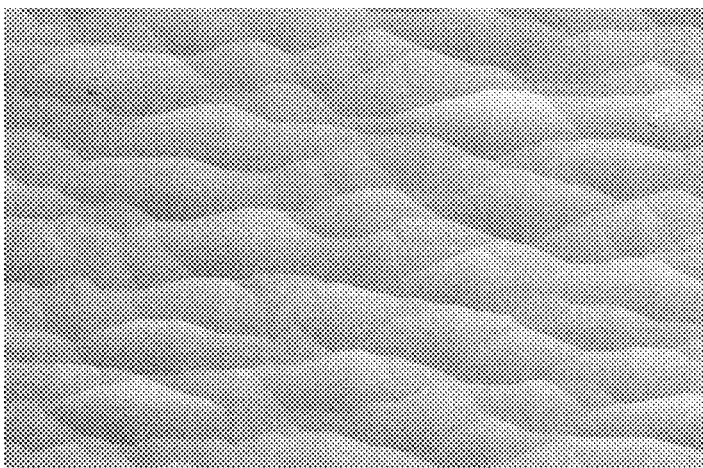
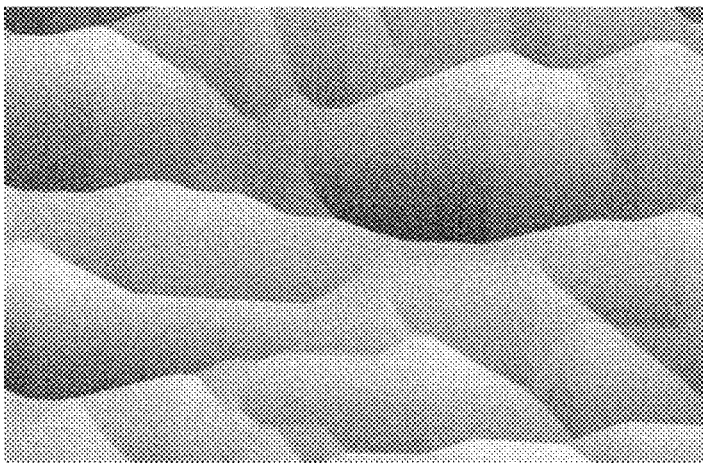


Fig. 11D

*Fig. 12**Fig. 13*

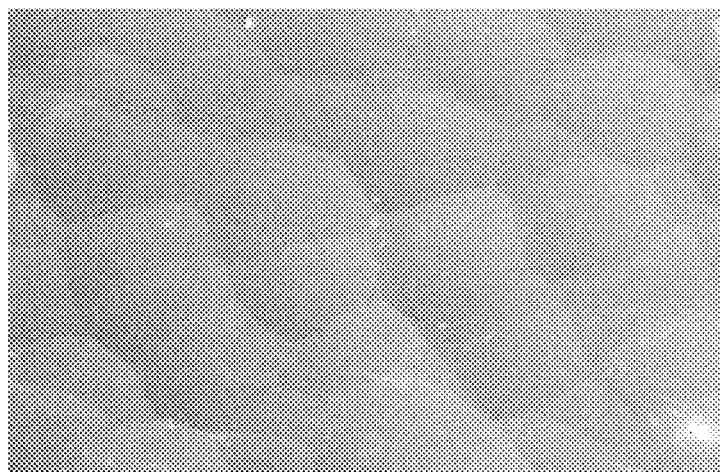
*Fig. 14**Fig. 15*

*Fig. 16**Fig. 17*

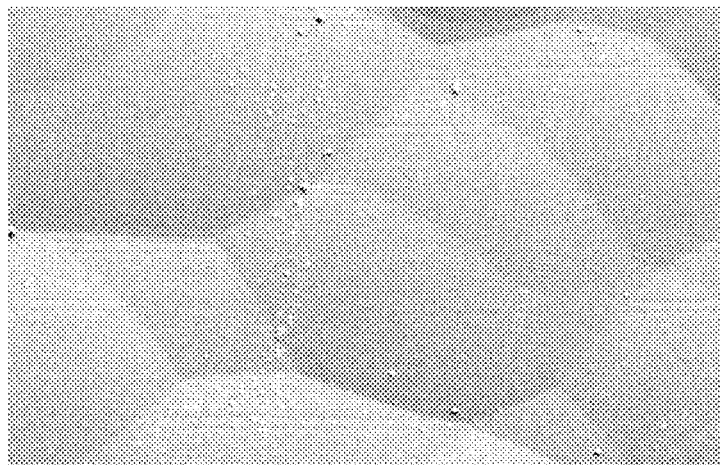
*Fig. 18A**Fig. 18B**Fig. 18C*



500 μm

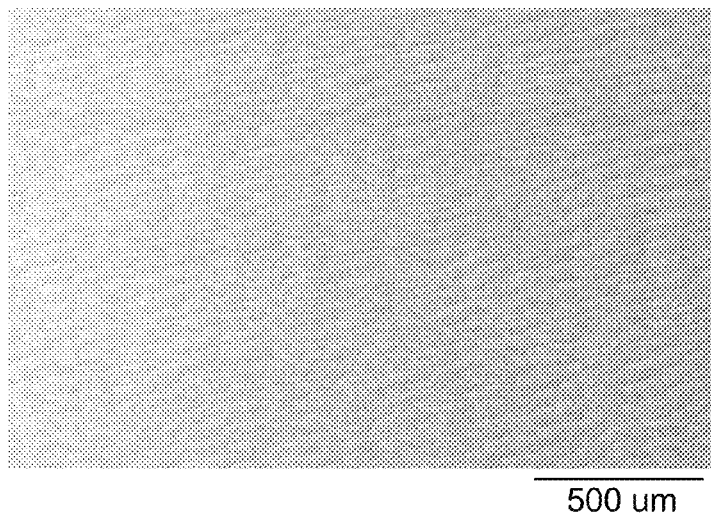
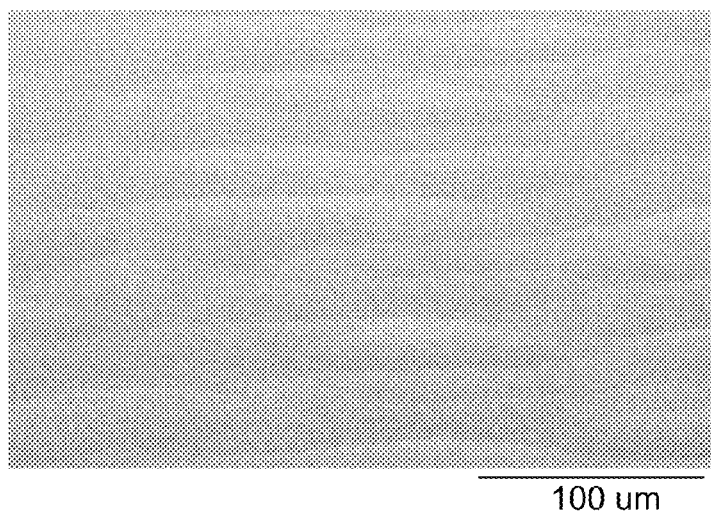
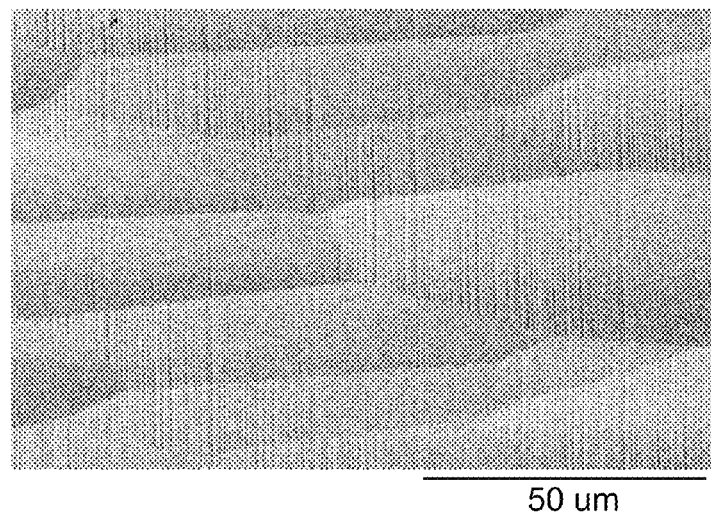
Fig. 19A

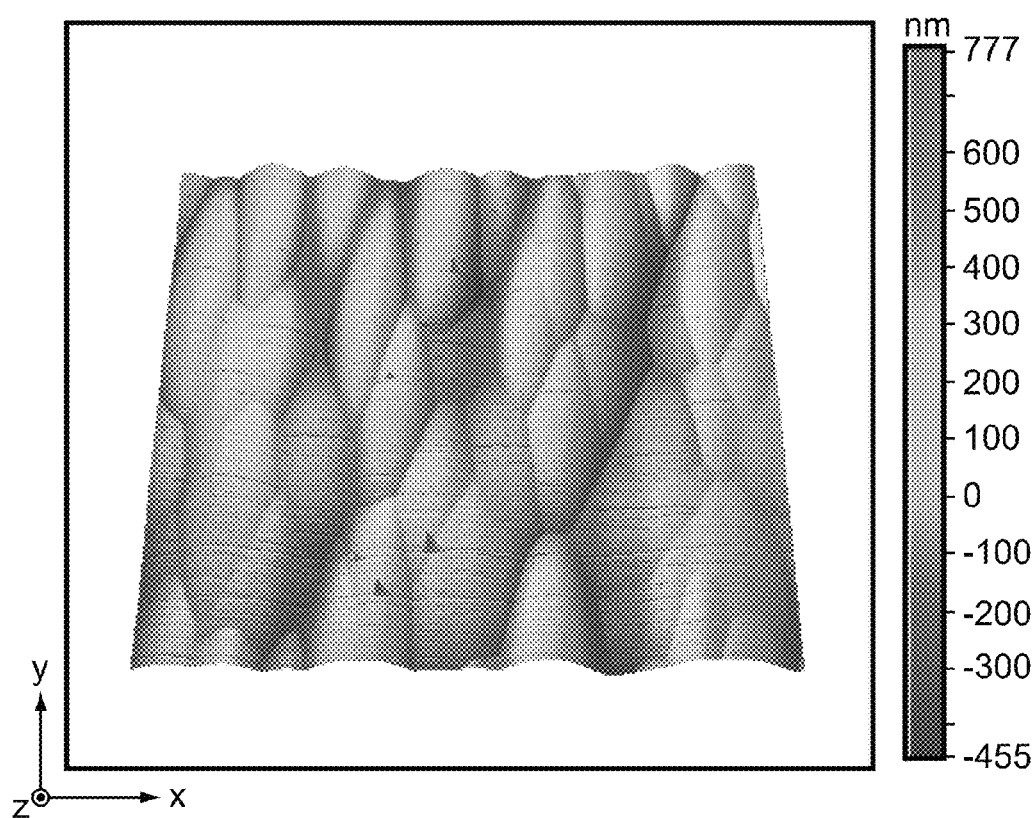
100 μm

Fig. 19B

50 μm

Fig. 19C

*Fig. 20A**Fig. 20B**Fig. 20C*

*Fig. 21*

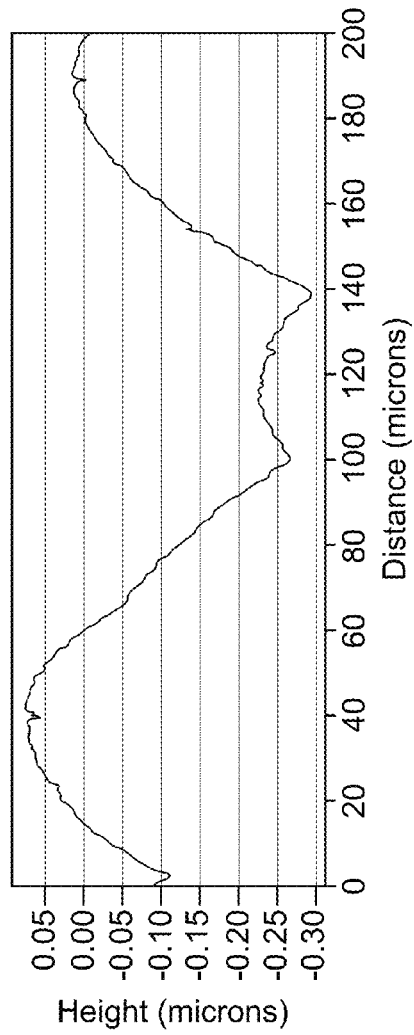


Fig. 22A

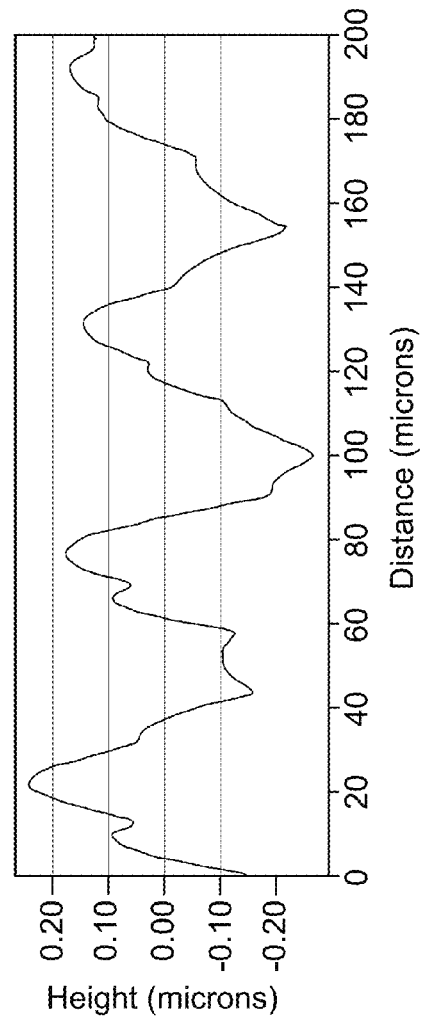


Fig. 22B

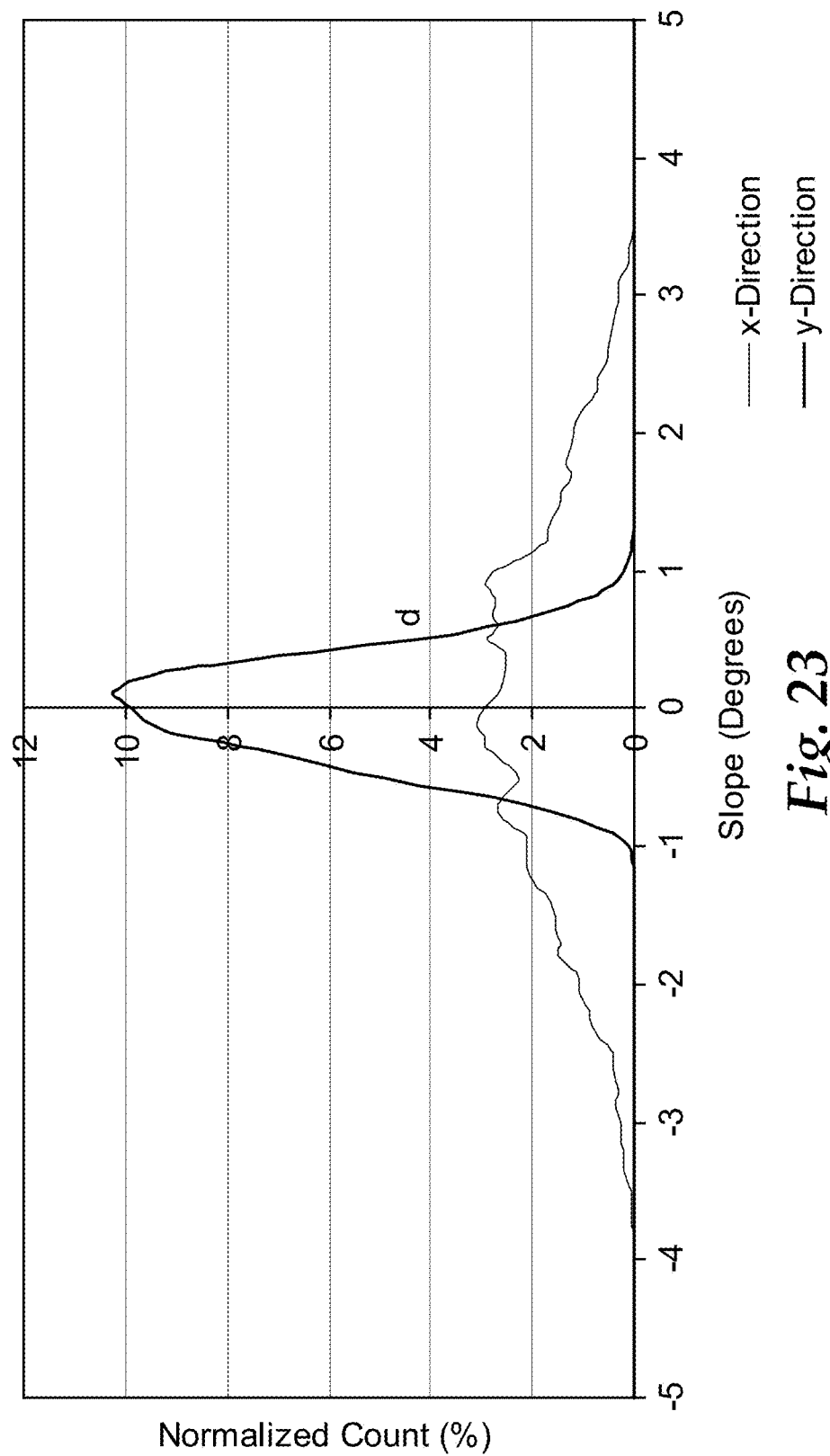


Fig. 23

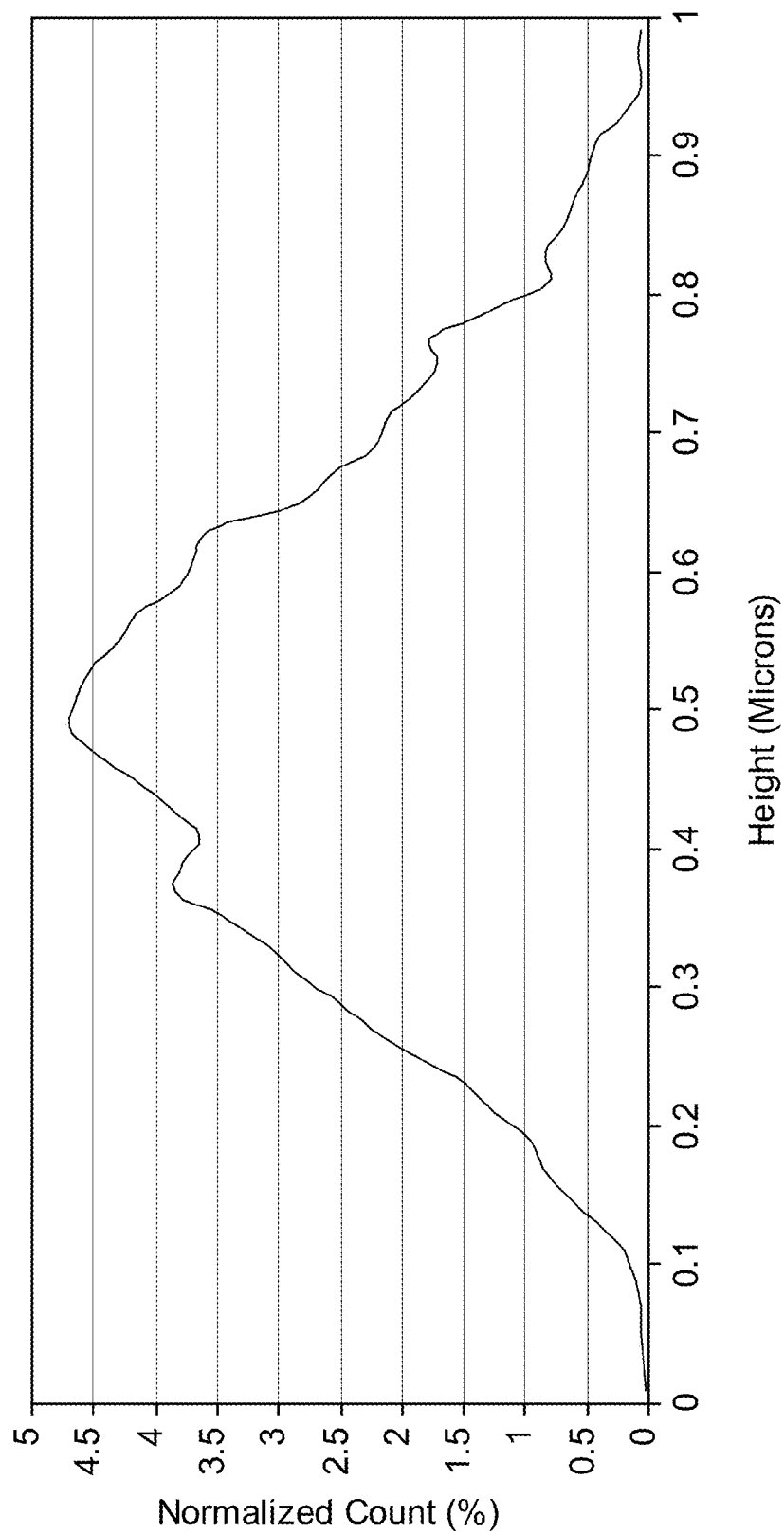
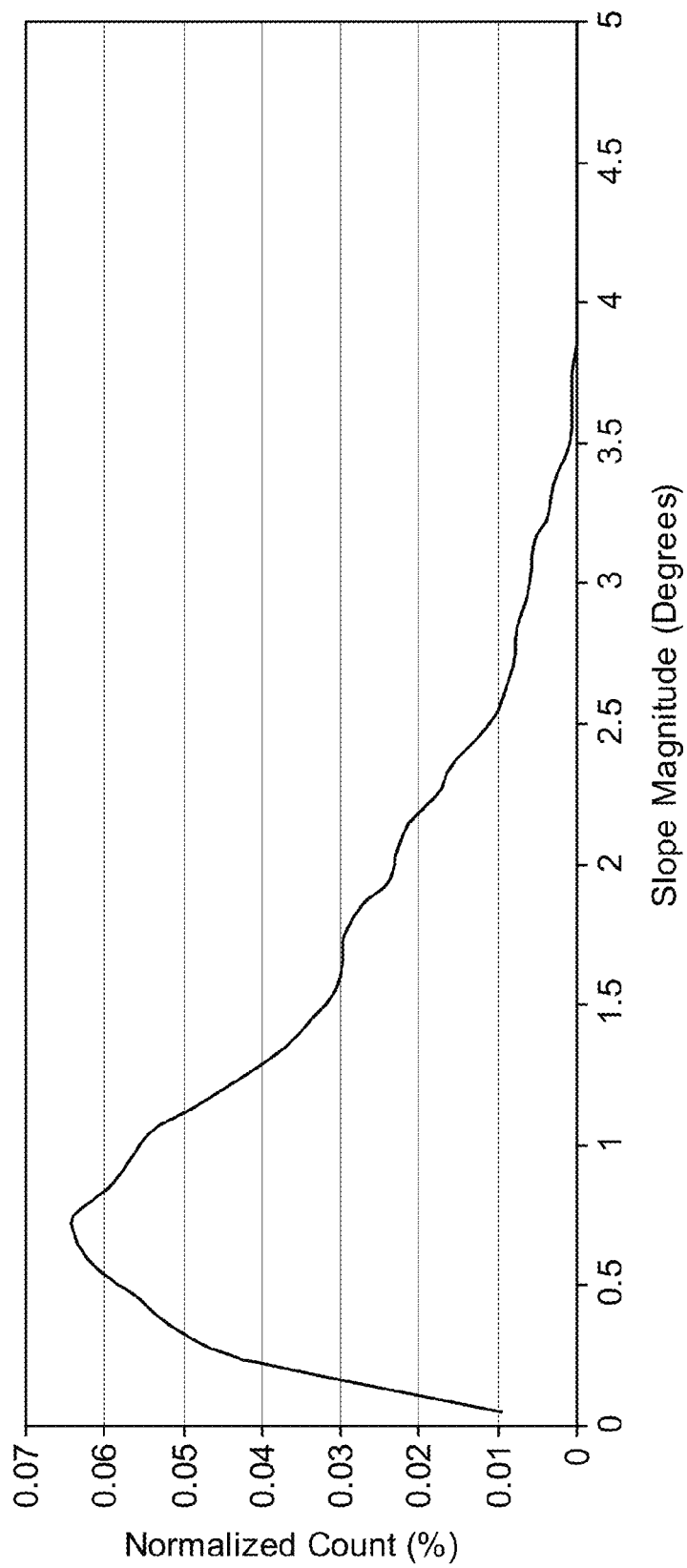
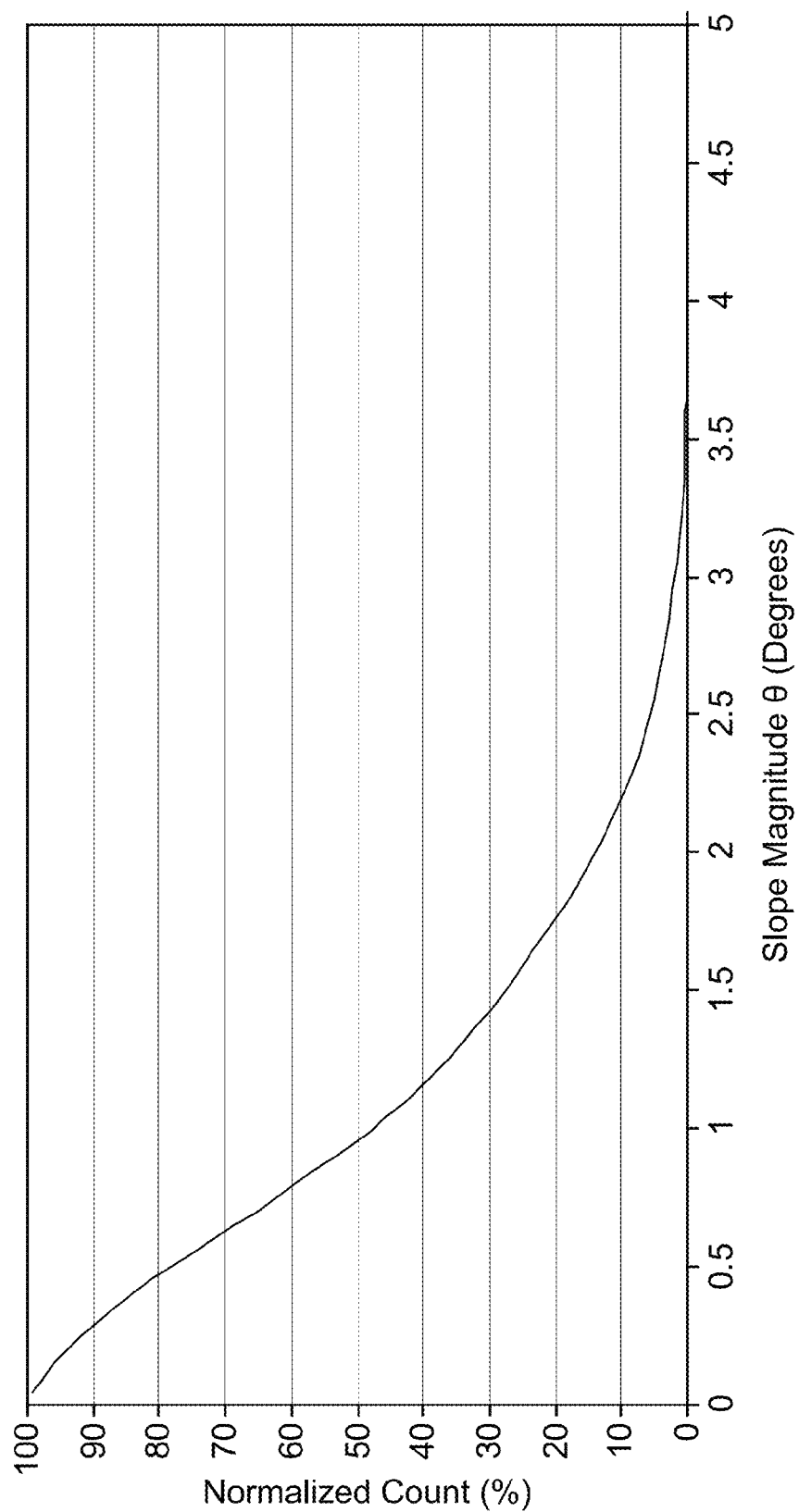


Fig. 24

*Fig. 25*

*Fig. 26*

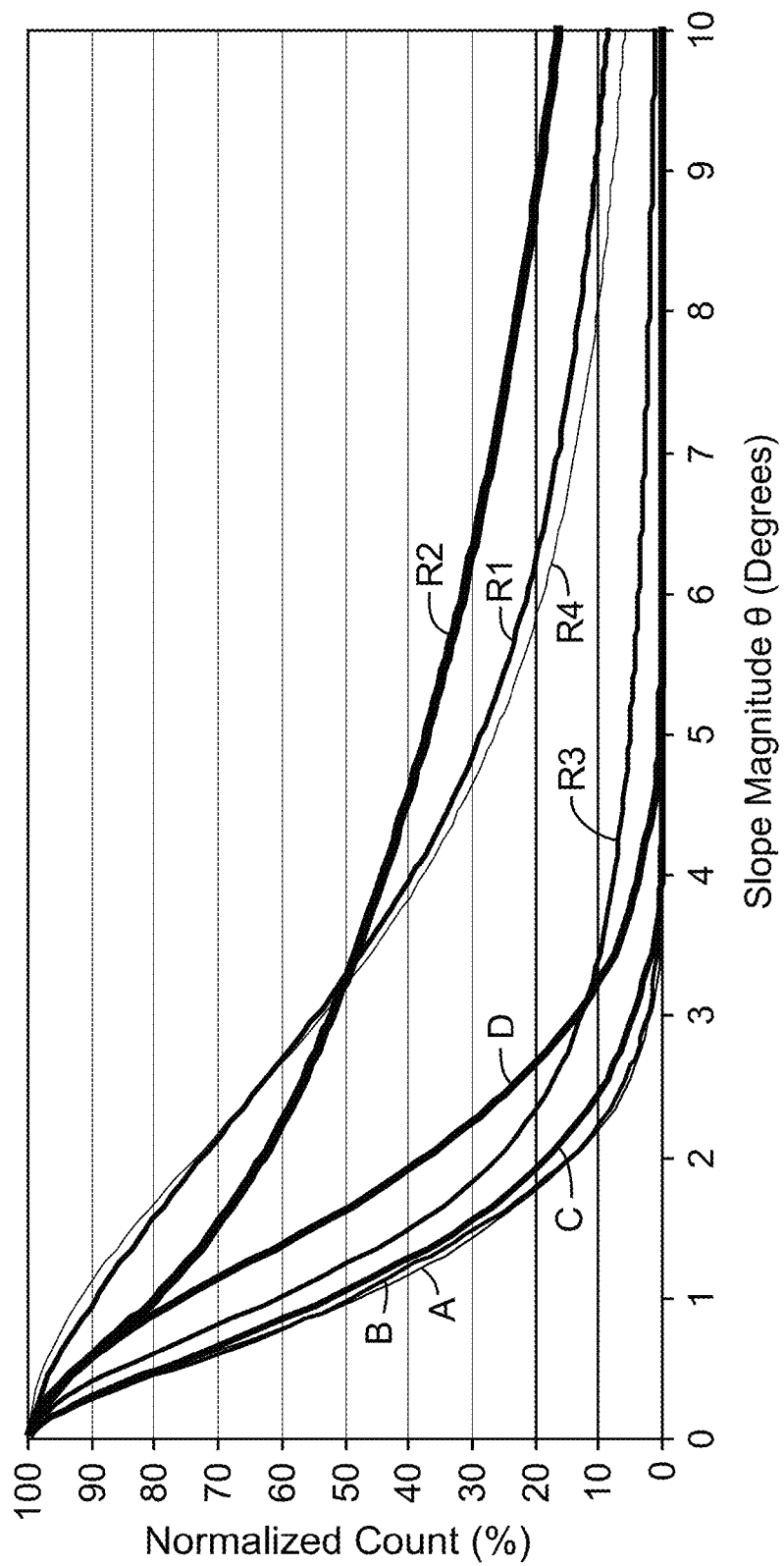
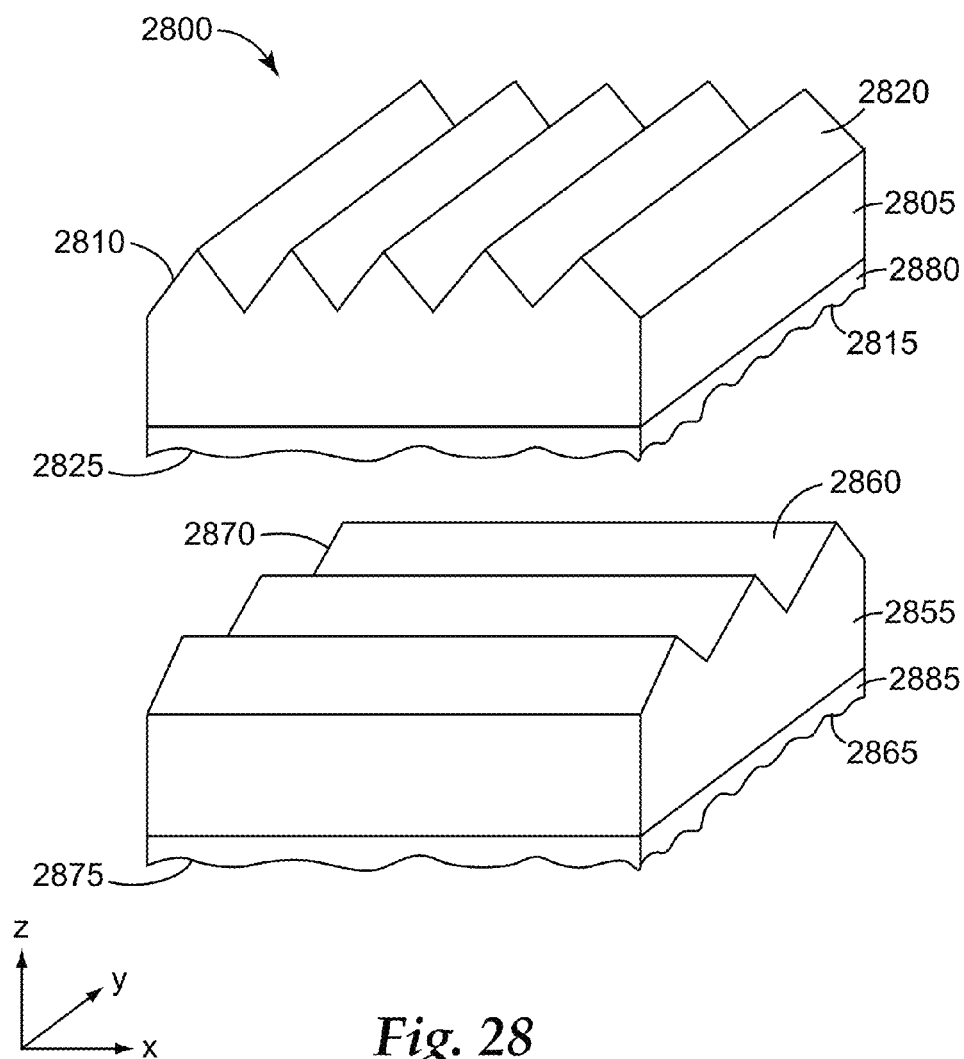


Fig. 27



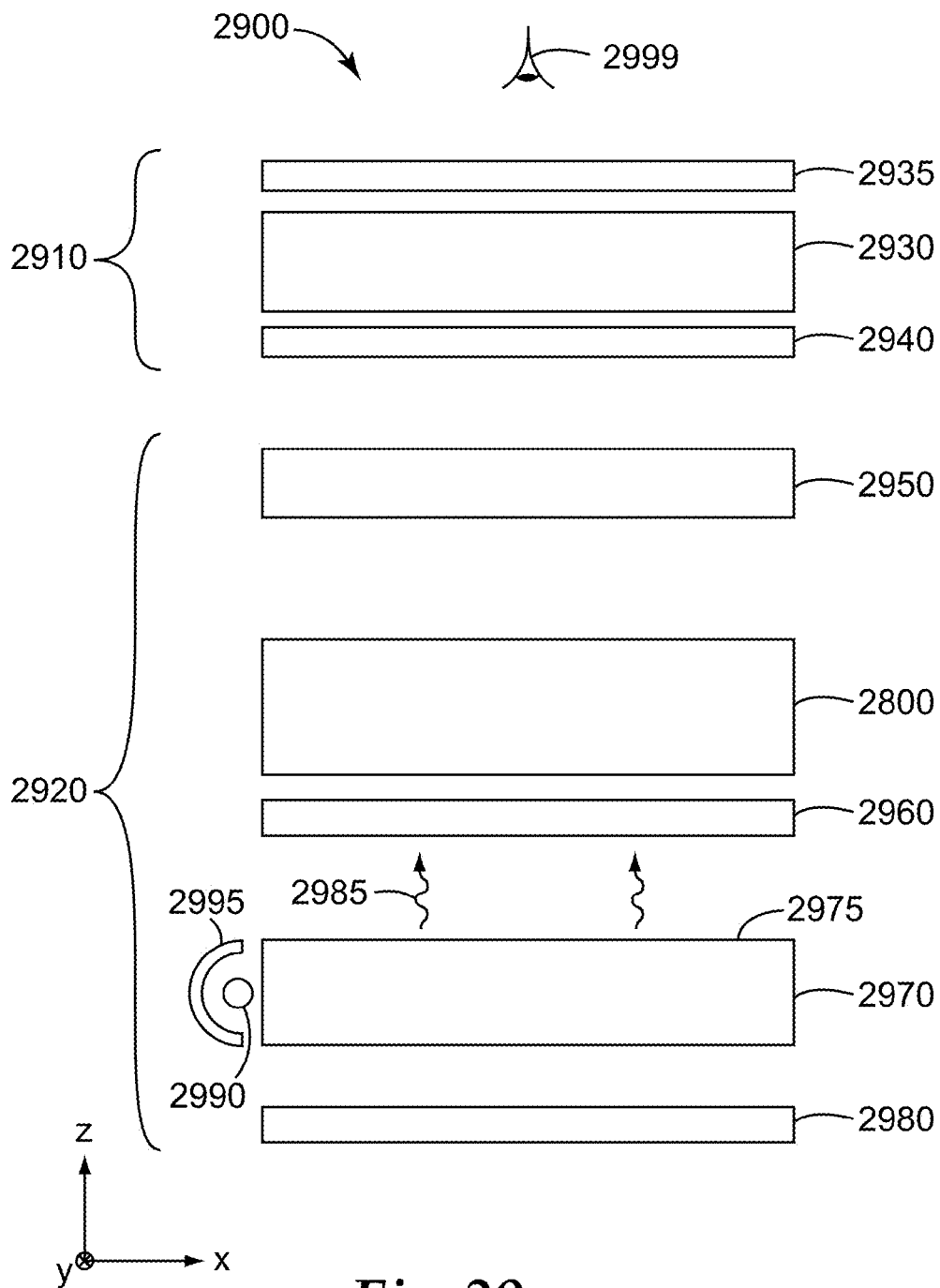


Fig. 29

1

LIGHT REDIRECTING FILM AND DISPLAY SYSTEM INCORPORATING SAME

CROSS REFERENCE TO RELATED APPLICATIONS

This application is a continuation of U.S. National Stage application Ser. No. 13/375,271, filed on Jan. 24, 2012, which is a U.S. National Stage filing under 35 U.S.C. 371 of PCT/US2010/036018, filed on May 25, 2010, which claim priority to U.S. Provisional Application No. 61/183,154, filed on Jun. 2, 2009, the disclosure of which are incorporated by reference in their entirety herein.

FIELD OF THE INVENTION

This invention generally relates to optical films for redirecting light. The invention is further applicable to optical systems, such as display systems, incorporating such optical films.

BACKGROUND

Display systems, such as liquid crystal display (LCD) systems, are used in a variety of applications and commercially available devices such as, for example, computer monitors, personal digital assistants (PDAs), mobile phones, miniature music players, and thin LCD televisions. Most LCDs include a liquid crystal panel and an extended area light source, often referred to as a backlight, for illuminating the liquid crystal panel. Backlights typically include one or more lamps and a number of light management films such as, for example, lightguides, mirror films, light redirecting films, retarder films, light polarizing films, and diffuser films. Diffuser films are typically included to hide optical defects and improve the brightness uniformity of the light emitted by the backlight.

SUMMARY OF THE INVENTION

Generally, the present invention relates to light redirecting films. In one embodiment, a light redirecting film includes a first major surface that includes a plurality of first microstructures that extend along a first direction. The light redirecting film also includes a second major surface that is opposite to the first major surface and includes a plurality of second microstructures. The second major surface has an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%. The light redirecting film has an average effective transmission that is not less than about 1.75. In some cases, the plurality of first microstructures include a plurality of linear prisms that extend along the first direction. In some cases, the maximum height of a microstructure in the plurality of first microstructures is different than the maximum height of another microstructure in the plurality of first microstructures. In some cases, the height of a microstructure in the plurality of first microstructures varies along the first direction. The plurality of second microstructures can include protrusions and/or recessions. In some cases, the plurality of second microstructures covers at least about 80%, or at least about 85%, or at least about 90%, or at least about 95%, of the second major surface. The plurality of second microstructures can form regular or irregular patterns. In some cases, no more than about 7%, or no more than about 5%, or no more than about 3%, of the second major surface has a slope magnitude that is greater than about 3.5 degrees. In some cases, no more than about 4%, or no more than about 2%, or no more than about 1%, of the second major surface

2

has a slope magnitude that is greater than about 5 degrees. In some cases, the second microstructures are not formed primarily by any particles that the light redirecting film may include. In some cases, the light redirecting film does not include particles that have an average size greater than about 0.5 microns. In some cases, the microstructures in the plurality of second microstructures have a slope distribution that has a half width half maximum (HWHM) that is not greater than about 6 degrees. In some cases, the light redirecting film includes a substrate layer that has opposing first and second major surfaces, a first layer that is disposed on the first major surface of the substrate layer and includes the first major surface of the light redirecting film, and a matte layer that is disposed on the second major surface of the substrate layer and includes the second major surface of the light redirecting layer. In some cases, the first layer has an index of refraction that is not less than about 1.6. In some cases, the matte layer includes a plurality of particles that have an average size that is less than the average size of the plurality of second microstructures by at least a factor of 5. In some cases, if the matte layer includes particles, then the average thickness of the matte layer is at least 2 microns greater than the average size of the particles. In some cases, if the matte layer includes particles, then the average thickness of the matte layer is greater than the average size of the particles by at least a factor of 2.

In another embodiment, a light redirecting film includes a first major surface that includes a plurality of linear microstructures, and a second major surface that is opposite to the first major surface and includes a plurality of second microstructures. The second major surface has an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%. The average effective transmission of the light redirecting film is not less, or is less by no more, than about 1.5% as compared to a light redirecting film that has the same construction except for comprising a smooth second major surface. In some cases, the plurality of second microstructures has geometrical symmetry and asymmetric slope distribution. In some cases, the plurality of second microstructures includes geometrical asymmetry and symmetric slope distribution.

In another embodiment, an optical stack includes a first light redirecting film that includes a first major surface and an opposing second major surface, where the first major surface includes a first plurality of microstructures that extend along a first direction, and the second major surface includes a second plurality of microstructures. The optical stack also includes a second light redirecting film that includes a third major surface and an opposing fourth major surface, where the third major surface faces the second major surface of the first light redirecting film and includes a third plurality of microstructures that extend along a second direction that is different than the first direction, and the fourth major surface includes a fourth plurality of microstructures. Each of the second and fourth major surfaces has an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%. In some cases, the optical stack has an average effective transmission that is not less than about 2.5.

In another embodiment, an optical stack includes a first light redirecting film that includes a first major surface and an opposing second major surface, where the first major surface includes a first plurality of microstructures that extend along a first direction. The optical stack also includes a second light redirecting film that includes a third major surface and an opposing fourth major surface, where the third major surface faces the second major surface of the first light redirecting

3

film and includes a third plurality of microstructures that extend along a second direction that is different than the first direction. Each of the second and fourth major surfaces has an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%. The average effective transmission of the optical stack is not less or is less by no more than about 1% as compared to an optical stack that has the same construction except for including smooth second and fourth major surfaces. In some cases, the optical stack has an average effective transmission that is not less as compared to an optical stack that has the same construction except for including smooth second and fourth major surfaces.

In another embodiment, an optical film includes a structured major surface that has geometrical symmetry and asymmetric slope distribution. In some cases, the optical film has an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%.

In another embodiment, an optical film includes a structured major surface that has geometrical asymmetry and symmetric slope distribution. In some cases, the optical film has an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%.

BRIEF DESCRIPTION OF DRAWINGS

The invention may be more completely understood and appreciated in consideration of the following detailed description of various embodiments of the invention in connection with the accompanying drawings, in which:

FIG. 1 is a schematic side-view of a light redirecting film;

FIG. 2 is a schematic side-view of an optical system for measuring effective transmission;

FIG. 3A is a schematic side-view of recessed microstructures;

FIG. 3B is a schematic side-view of protruding microstructures;

FIG. 4A is a schematic top-view of regularly arranged microstructures;

FIG. 4B is a schematic top-view of irregularly arranged microstructures;

FIG. 5 is a schematic side-view of a microstructure;

FIG. 6 is calculated optical haze versus surface fraction "P";

FIG. 7 is calculated optical clarity versus surface fraction "P";

FIG. 8 is a schematic side-view of an optical film;

FIG. 9 is a schematic side-view of another optical film;

FIG. 10 is a schematic side-view of a cutting tool system;

FIGS. 11A-11D are schematic side-views of various cutters;

FIGS. 12-17 are optical micrographs of various microstructured surfaces;

FIGS. 18A, 18B and 18C are SEM images of various microstructured surfaces at different magnifications;

FIGS. 19A, 19B and 19C are SEM images of various microstructured surfaces at different magnifications;

FIGS. 20A, 20B and 20C are SEM images of various microstructured surfaces at different magnifications;

FIG. 21 is an AFM surface profile of a microstructured surface;

FIG. 22A-22B are cross-sectional profiles of the microstructured surface in FIG. 21 along two mutually orthogonal directions;

FIG. 23 is percent slope distribution for the microstructured surface in FIG. 21 along two mutually orthogonal directions;

4

FIG. 24 is percent height distribution for the microstructured surface in FIG. 21;

FIG. 25 is percent slope magnitude distribution for the microstructured surface in FIG. 21;

FIG. 26 is percent cumulative slope distribution for the microstructured surface in FIG. 21;

FIG. 27 is percent cumulative slope distributions for various microstructured surfaces;

FIG. 28 is a schematic side-view of an optical stack; and

FIG. 29 is a schematic side-view of a display system.

In the specification, a same reference numeral used in multiple figures refers to the same or similar elements having the same or similar properties and functionalities.

DETAILED DESCRIPTION

This invention generally relates to light redirecting films that are capable of substantially enhancing brightness in a display system while at the same time masking and/or eliminating physical defects such as scratches, and undesirable optical effects such as moiré and color mora. The disclosed light redirecting films include an array of linear microstructures for improving brightness and a matte surface for improving the display cosmetics. The optical haze of the matte surface is sufficiently low to maintain brightness, and the optical clarity of the matte surface is sufficiently low to mask and/or eliminate defects.

FIG. 1 is a schematic side-view of a light redirecting film **100** for redirecting an incident light toward a desired direction. Light redirecting film **100** includes a first major surface **110** that includes a plurality of microstructures **150** that extend along the y-direction. Light redirecting film **100** also includes a second major surface **120** that is opposite first major surface **110** and includes a plurality of microstructures **160**.

Light redirecting film **100** also includes a substrate layer **170** that is disposed between respective first and second major surfaces **110** and **120** and includes a first major surface **172** and an opposing second major surface **174**. Light redirecting film **100** also includes a prism layer **130** that is disposed on first major surface **172** of the substrate layer and includes first major surface **110** of the light redirecting film, and a matte layer **140** that is disposed on second major surface **174** of the substrate layer and includes second major surface **120** of the light redirecting film. The matte layer has a major surface **142** opposite major surface **120**.

The exemplary light redirecting film **100** includes three layers **130**, **170** and **140**. In general, the light redirecting film can have one or more layers. For example, in some cases, the light redirecting film can have a single layer that includes respective first and second major surfaces **110** and **120**. As another example, in some cases, the light redirecting film can have many layers. For example, in such cases, substrate **170** can have multiple layers.

Microstructures **150** are primarily designed to redirect light that is incident on major surface **120** of the light redirecting film, along a desired direction, such as along the positive z-direction. In the exemplary light redirecting film **100**, microstructures **150** are prismatic linear structures. In general, microstructures **150** can be any type microstructures that are capable of redirecting light by, for example, refracting a portion of an incident light and recycling a different portion of the incident light. For example, the cross-sectional profiles of microstructures **150** can be or include curved and/or piecewise linear portions. For example, in some cases, microstructures **150** can be linear cylindrical lenses extending along the y-direction.

Each linear prismatic microstructure **150** includes an apex angle **152** and a height **154** measured from a common reference plane such as, for example, major plane surface **172**. In some cases, such as when it is desirable to reduce optical coupling or wet-out and/or improve durability of the light redirecting film, the height of a prismatic microstructure **150** can change along the y-direction. For example, the prism height of prismatic linear microstructure **151** varies along the y-direction. In such cases, prismatic microstructure **151** has a local height that varies along the y-direction, a maximum height **155**, and an average height. In some cases, a prismatic linear microstructure, such as linear microstructure **153**, has a constant height along the y-direction. In such cases, the microstructure has a constant local height that is equal to the maximum height and the average height.

In some cases, such as when it is desirable to reduce optical coupling or wet-out, some of the linear microstructures are shorter and some of the linear microstructures are taller. For example, height **156** of linear microstructure **153** is smaller than height **158** of linear microstructure **157**.

Apex or dihedral angle **152** can have any value that may be desirable in an application. For example, in some cases, apex angle **152** can be in a range from about 70 degrees to about 110 degrees, or from about 80 degrees to about 100 degrees, or from about 85 degrees to about 95 degrees. In some cases, microstructures **150** have equal apex angles which can, for example, be in a range from about 88 or 89 degree to about 92 or 91 degrees, such as 90 degrees.

Prism layer **130** can have any index of refraction that may be desirable in an application. For example, in some cases, the index of refraction of the prism layer is in a range from about 1.4 to about 1.8, or from about 1.5 to about 1.8, or from about 1.5 to about 1.7. In some cases, the index of refraction of the prism layer is not less than about 1.5, or not less than about 1.55, or not less than about 1.6, or not less than about 1.65, or not less than about 1.7.

In some cases, such as when light redirecting film **100** is used in a liquid crystal display system, the light redirecting film **100** can increase or improve the brightness of the display. In such cases, the light redirecting film has an effective transmission or relative gain that is greater than 1. As used herein, effective transmission is the ratio of the luminance of the display system with the film in place in the display system to the luminance of the display without the film in place.

Effective transmission (ET) can be measured using optical system **200**, a schematic side-view of which is shown in FIG. 2. Optical system **200** is centered on an optical axis **250** and includes a hollow lambertian light box that emits a lambertian light **215** through an emitting or exit surface **212**, a linear light absorbing polarizer **220**, and a photo detector **230**. Light box **210** is illuminated by a stabilized broadband light source **260** that is connected to an interior **280** of the light box via an optical fiber **270**. A test sample the ET of which is to be measured by the optical system, is placed at location **240** between the light box and the absorbing linear polarizer.

The ET of light redirecting film **100** can be measured by placing the light redirecting film in location **240** with linear prisms **150** facing the photo detector and microstructures **160** facing the light box. Next, the spectrally weighted axial luminance I_1 (luminance along optical axis **250**) is measured through the linear absorbing polarizer by the photo detector. Next, the light redirecting film is removed and the spectrally weighted luminance I_2 is measured without the light redirecting film placed at location **240**. ET is the ratio I_1/I_2 . ET0 is the effective transmission when linear prisms **150** extend along a direction that is parallel to the polarizing axis of linear absorbing polarizer **220**, and ET90 is the effective transmission

when linear prisms **150** extend along a direction that is perpendicular to the polarizing axis of the linear absorbing polarizer. The average effective transmission (ETA) is the average of ET0 and ET90.

Effective transmission values disclosed herein were measured using a SpectraScan™ PR-650 SpectraColorimeter (available from Photo Research, Inc, Chatsworth, Calif.) for photo detector **230**. Light box **210** was a Teflon cube with a total reflectance of about 85%.

In some cases, such as when light redirecting film **100** is used in a display system to increase the brightness and the linear prisms have an index of refraction that is greater than about 1.6, the average effective transmission (ETA) of the light redirecting film is not less than about 1.5, or not less than about 1.55, or not less than about 1.6, or not less than about 1.65, or not less than about 1.7, or not less than about 1.75, or not less than about 1.8, or not less than about 1.85.

Microstructures **160** in matte layer **140** are primarily designed to hide undesirable physical defects (such as, for example, scratches) and/or optical defects (such as, for example, undesirably bright or "hot" spots from a lamp in a display or illumination system) with no, or very little adverse, effect on the capabilities of the light redirecting film to redirect light and enhance brightness. In such cases, second major surface **120** has an optical haze that is not greater than about 5%, or not greater than about 4.5%, or not greater than about 4%, or not greater than about 3.5%, or not greater than about 3%, or not greater than about 2.5%, or not greater than about 2%, or not greater than about 1.5%, or not greater than about 1%; and an optical clarity that is not greater than about 85%, or not greater than about 80%, or not greater than about 75%, or not greater than about 70%, or not greater than about 65%, or not greater than about 60%.

Optical haze, as used herein, is defined as the ratio of the transmitted light that deviates from the normal direction by more than 4 degrees to the total transmitted light. Haze values disclosed herein were measured using a Haze-Gard Plus haze meter (available from BYK-Gardiner, Silver Springs, Md.) according to the procedure described in ASTM D1003. Optical clarity, as used herein, refers to the ratio $(T_1 - T_2)/(T_1 + T_2)$, where T_1 is the transmitted light that deviates from the normal direction between 1.6 and 2 degrees from the normal direction, and T_2 is the transmitted light that lies between zero and 0.7 degrees from the normal direction. Clarity values disclosed herein were measured using a Haze-Gard Plus haze meter from BYK-Gardiner.

Microstructures **160** can be any type microstructures that may be desirable in an application. In some cases, microstructures **160** can be recessions. For example, FIG. 3A is a schematic side-view of a matte layer **310** that is similar to matte layer **140** and includes recessed microstructures **320**. In some cases, microstructures **160** can be protrusions. For example, FIG. 3B is a schematic side-view of a matte layer **330** that is similar to matte layer **140** and includes protruding microstructures **340**.

In some cases, microstructures **160** form a regular pattern. For example, FIG. 4A is a schematic top-view of microstructures **410** that are similar to microstructures **160** and form a regular pattern in a major surface **415**. In some cases, microstructures **160** form an irregular pattern. For example, FIG. 4B is a schematic top-view of microstructures **420** that are similar to microstructures **160** and form an irregular pattern. In some cases, microstructures **160** form a pseudo-random pattern that appears to be random.

In general, microstructures **160** can have any height and any height distribution. In some cases, the average height (that is, the average maximum height minus the average mini-

num height) of microstructures **160** is not greater than about 5 microns, or not greater than about 4 microns, or not greater than about 3 microns, or not greater than about 2 microns, or not greater than about 1 micron, or not greater than about 0.9 microns, or not greater than about 0.8 microns, or not greater than about 0.7 microns.

FIG. 5 is a schematic side view of a portion of matte layer **140**. In particular, FIG. 5 shows a microstructure **160** in major surface **120** and facing major surface **142**. Microstructure **160** has a slope distribution across the surface of the microstructure. For example, the microstructure has a slope θ at a location **510** where θ is the angle between normal line **520** which is perpendicular to the microstructure surface at location **510** ($\alpha=90$ degrees) and tangent line **530** which is tangent to the microstructure surface at the same location. Slope θ is also the angle between tangent line **530** and major surface **142** of the matte layer.

Optical haze and clarity of matte layer **140** were calculated using a program that was similar to commercially available ray tracing programs such as, for example, TracePro (available from Lambda Research Corp., Littleton, Mass.). In carrying out the calculations, it was assumed that each microstructure had a Gaussian slope distribution with a half width at half maximum (HWHM) equal to σ . It was further assumed that the matte layer had an index of refraction equal to 1.5. The calculated results are shown in FIGS. 6 and 7. FIG. 6 is the calculated optical haze versus surface fraction “f” for nine different values of σ , where f is percent area of major surface **120** covered by microstructures **160**. FIG. 7 is the calculated optical clarity versus f. In some cases, such as when microstructures **160** effectively hide physical and/or optical defects without reducing or reducing very little the brightness, the plurality of microstructures **160** covers at least about 70%, or at least about 75%, or at least about 80%, or at least about 85%, or at least about 90%, or at least about 95%, of second major surface **120**. In some cases, such as when the microstructures have a Gaussian or normal slope distribution, the HWHM σ of the distribution is not greater than about 4.5 degrees, or not greater than about 4 degrees, or not greater than about 3.5 degrees, or not greater than about 3 degrees, or not greater than about 2.5 degrees, or not greater than about 2 degrees.

In the exemplary calculations disclosed above, it was assumed that microstructures **160** have a Gaussian slope distribution with a HWHM equal to σ . In general, the microstructures can have any distribution that may be desirable in an application. For example, in some cases, such as when the microstructures are spherical segments, the microstructures can have a uniform distribution between two limiting angles. Other exemplary slope distributions include Lorentzian distributions, parabolic distributions, and combinations of different, such as Gaussian, distributions. For example, in some cases, the microstructures can have a first Gaussian distribution with a smaller HWHM σ_1 added to, or combined with, a second Gaussian distribution with a larger HWHM σ_2 . In some cases, the microstructures can have asymmetric slope distributions. In some cases, the microstructures can have symmetric distributions.

FIG. 8 is a schematic side-view of an optical film **800** that includes a matte layer **860** disposed on a substrate **850** similar to substrate **170**. Matte layer **860** includes a first major surface **810** attached to substrate **850**, a second major surface **820** opposite the first major surface, and a plurality of particles **830** dispersed in a binder **840**. Second major surface **820** includes a plurality of microstructures **870**. A substantial portion, such as at least about 50%, or at least about 60%, or at least about 70%, or at least about 80%, or at least about

90%, of microstructures **870** are disposed on and formed primarily because of particles **830**. In other words, particles **830** are the primary reason for the formation of microstructures **870**. In such cases, particles **830** have an average size that is greater than about 0.25 microns, or greater than about 0.5 microns, or greater than about 0.75 microns, or greater than about 1 micron, or greater than about 1.25 microns, or greater than about 1.5 microns, or greater than about 1.75 microns, or greater than about 2 microns.

In some cases, matte layer **140** can be similar to matte layer **860** and can include a plurality of particles that are the primary reason for the formation of microstructures **160** in second major surface **120**.

Particles **830** can be any type particles that may be desirable in an application. For example, particles **830** may be made of polymethyl methacrylate (PMMA), polystyrene (PS), or any other material that may be desirable in an application. In general, the index of refraction of particles **830** is different than the index of refraction of binder **840**, although in some cases, they may have the same refractive indices. For example, particles **830** can have an index of refraction of about 1.35, or about 1.48, or about 1.49, or about 1.50, and binder **840** can have an index of refraction of about 1.48, or about 1.49, or about 1.50.

In some cases, matte layer **140** does not include particles. In some cases, matte layer **140** includes particles, but the particles are not the primary reason for the formation of microstructures **160**. For example, FIG. 9 is a schematic side-view of an optical film **900** that includes a matte layer **960** similar to matter layer **140** disposed on a substrate **950** similar to substrate **170**. Matte layer **960** includes a first major surface **910** attached to substrate **950**, a second major surface **920** opposite the first major surface, and a plurality of particles **930** dispersed in a binder **940**. Second major surface **970** includes a plurality of microstructures **970**. Even though matte layer **960** includes particles **930**, the particles are not the primary reason for the formation of microstructures **970**. For example, in some cases, the particles are much smaller than the average size of the microstructures. In such cases, the microstructures can be formed by, for example, microreplicating a structured tool. In such cases, the average size of particles **930** is less than about 0.5 microns, or less than about 0.4 microns, or less than about 0.3 microns, or less than about 0.2 microns, or less than about 0.1 microns. In such cases, a substantial fraction, such as at least about 50%, or at least about 60%, or at least about 70%, or at least about 80%, or at least about 90%, of microstructures **970** are not disposed on particles that have an average size that is greater than about 0.5 microns, or greater than about 0.75 microns, or greater than about 1 micron, or greater than about 1.25 microns, or greater than about 1.5 microns, or greater than about 1.75 microns, or greater than about 2 microns. In some cases, the average size of particles **930** is less than the average size of microstructures **930** by at least a factor of about 2, or at least a factor of about 3, or at least a factor of about 4, or at least a factor of about 5, or at least a factor of about 6, or at least a factor of about 7, or at least a factor of about 8, or at least a factor of about 9, or at least a factor of about 10. In some cases, if matte layer **960** includes particles **930**, then matte layer **960** has an average thickness “t” that is greater than the average size of the particles by at least about 0.5 microns, or at least about 1 micron, or at least about 1.5 microns, or at least about 2 microns, or at least about 2.5 microns, or at least about 3 microns. In some cases, if the matte layer includes a plurality of particles then the average thickness of the matte layer is greater than the average thickness of the particles by at least a factor of about 2, or at least a factor of about 3, or at least a

factor of about 4, or at least a factor of about 5, or at least a factor of about 6, or at least a factor of about 7, or at least a factor of about 8, or at least a factor of about 9, or at least a factor of about 10.

Referring back to FIG. 1, in some cases, light redirecting film **100** has small particles in at least some of the layers, such as prism layer **130**, substrate layer **170**, or matte layer **140**, for increasing the index of refraction of the layer. For example, one or more layers in light redirecting film **100** can include inorganic nanoparticles such as silica or zirconia nanoparticles discussed in, for example U.S. Pat. No. 7,074,463 (Jones et al.) and U.S. Patent Publication No. 2006/0210726. In some cases, light redirecting film **100** does not include any particles having an average size that is greater than about 2 microns, or about 1.5 microns, or about 1 micron, or about 0.75 microns, or about 0.5 microns, or about 0.25 microns, or about 0.2 microns, or about 0.15 microns, or about 0.1 microns.

Microstructures **160** can be made using any fabrication method that may be desirable in an application. For example, the microstructures can be fabricated using microreplication from a tool, where the tool may be fabricated using any available fabrication method, such as by using engraving or diamond turning. Exemplary diamond turning systems and methods can include and utilize a fast tool servo (FTS) as described in, for example, PCT Published Application No. WO 00/48037, and U.S. Pat. Nos. 7,350,442 and 7,328,638, the disclosures of which are incorporated in their entireties herein by reference thereto.

FIG. 10 is a schematic side-view of a cutting tool system **1000** that can be used to cut a tool which can be microreplicated to produce microstructures **160** and matte layer **140**. Cutting tool system **1000** employs a thread cut lathe turning process and includes a roll **1010** that can rotate around and/or move along a central axis **1020** by a driver **1030**, and a cutter **1040** for cutting the roll material. The cutter is mounted on a servo **1050** and can be moved into and/or along the roll along the x-direction by a driver **1060**. In general, cutter **1040** is mounted normal to the roll and central axis **1020** and is driven into the engraveable material of roll **1010** while the roll is rotating around the central axis. The cutter is then driven parallel to the central axis to produce a thread cut. Cutter **1040** can be simultaneously actuated at high frequencies and low displacements to produce features in the roll that when microreplicated result in microstructures **160**.

Servo **1050** is a fast tool servo (FTS) and includes a solid state piezoelectric (PZT) device, often referred to as a PZT stack, which rapidly adjusts the position of cutter **1040**. FTS **1050** allows for highly precise and high speed movement of cutter **1040** in the x-, y- and/or z-directions, or in an off-axis direction. Servo **1050** can be any high quality displacement servo capable of producing controlled movement with respect to a rest position. In some cases, servo **1050** can reliably and repeatedly provide displacements in a range from 0 to about 20 microns with about 0.1 micron or better resolution.

Driver **1060** can move cutter **1040** along the x-direction parallel to central axis **1020**. In some cases, the displacement resolution of driver **1060** is better than about 0.1 microns, or better than about 0.01 microns. Rotary movements produced by driver **1030** are synchronized with translational movements produced by driver **1060** to accurately control the resulting shapes of microstructures **160**.

The engraveable material of roll **1010** can be any material that is capable of being engraved by cutter **1040**. Exemplary roll materials include metals such as copper, various polymers, and various glass materials.

Cutter **1040** can be any type of cutter and can have any shape that may be desirable in an application. For example, FIG. 11A is a schematic side-view of a cutter **1110** that has an arc-shape cutting tip **1115** with a radius "R". In some cases, the radius R of cutting tip **1115** is at least about 100 microns, or at least about 150 microns, or at least about 200 microns, or at least about 300 microns, or at least about 400 microns, or at least about 500 microns, or at least about 1000 microns, or at least about 1500 microns, or at least about 2000 microns, or at least about 2500 microns, or at least about 3000 microns.

As another example, FIG. 11B is a schematic side-view of a cutter **1120** that has a V-shape cutting tip **1125** with an apex angle β . In some cases, the apex angle β of cutting tip **1125** is at least about 100 degrees, or at least about 110 degrees, or at least about 120 degrees, or at least about 130 degrees, or at least about 140 degrees, or at least about 150 degrees, or at least about 160 degrees, or at least about 170 degrees. As yet other examples, FIG. 11C is a schematic side-view of a cutter **1130** that has a piece-wise linear cutting tip **1135**, and FIG. 11D is a schematic side-view of a cutter **1140** that has a curved cutting tip **1145**.

Referring back to FIG. 10, the rotation of roll **1010** along central axis **1020** and the movement of cutter **1040** along the x-direction while cutting the roll material defines a thread path around the roll that has a pitch P_1 along the central axis. As cutter moves along a direction normal to the roll surface to cut the roll material, the width of the material cut by the cutter changes as the cutter moves or plunges in and out. Referring to, for example FIG. 11A, the maximum penetration depth by the cutter corresponds to a maximum width P_2 cut by the cutter. In some cases, such as when microstructures **160** in light redirecting film **100** are geometrically symmetric and sufficiently capable of hiding or masking physical and/or optical defects without reducing, or reducing very little, the brightness, the ratio P_2/P_1 is in a range from about 1.5 to about 6, or from about 2 to about 5, or from about 2.5 to about 4.

Several samples having microstructures similar to microstructures **160** were made using a cutting tool system similar to cutting tool system **1000** to make a patterned roll and subsequently microreplicating the patterned tool to make matte layers similar to matte layer **140**. FIG. 12 is a top-view optical micrograph of a sample that was made using a cutter similar to cutter **1110** where the radius of the cutting tip **1115** was about 480 microns. The sample was geometrically symmetric and had a symmetric slope distribution, where by geometrically symmetric it is meant that the average microstructure size along one direction, such as the x-direction, is substantially the same as the average microstructure size along an orthogonal direction, such as the y-direction. In particular, the sample had an average slope magnitude of about 1.18 degrees along the x-direction and an average slope magnitude of about 1.22 degrees along the y-direction. FIG. 13 is a top-view optical micrograph of a sample that was made using a cutter similar to cutter **1110** where the radius of the cutting tip **1115** was about 480 microns. The sample was geometrically symmetric and had an asymmetric slope distribution. In particular, the sample had an average slope magnitude of about 0.72 degrees along the x-direction and an average slope magnitude of about 1.11 degrees along the y-direction. FIG. 14 is a top-view optical micrograph of a sample that was made using a cutter similar to cutter **1110** where the radius of the cutting tip **1115** was about 3300 microns. The sample was geometrically asymmetric and had an asymmetric slope distribution. In particular, the sample had an average slope magnitude of about 0.07 degrees along the x-direction and an average slope magnitude of about 1.48 degrees along the y-direction. FIG. 15 is a top-view optical

11

micrograph of a sample that was made using a cutter similar to cutter 1110 where the radius of the cutting tip 1115 was about 3300 microns. The sample was geometrically asymmetric and had an asymmetric slope distribution. In particular, the sample had an average slope magnitude of about 0.18 degrees along the x-direction and an average slope magnitude of about 0.85 degrees along the y-direction. FIG. 16 is a top-view optical micrograph of a sample that was made using a cutter similar to cutter 1120 where the apex angle of the cutting tip 1125 was about 176 degrees. The sample was geometrically symmetric and had a symmetric slope distribution. In particular, the sample had an average slope magnitude of about 2.00 degrees along the x-direction and an average slope magnitude of about 1.92 degrees along the y-direction. FIG. 17 is a top-view optical micrograph of a sample that was made using a cutter similar to cutter 1120 where the apex angle of the cutting tip 1125 was about 175 degrees. The sample was geometrically asymmetric and had a symmetric slope distribution. In particular, the sample had an average slope magnitude of about 2.50 degrees along the x-direction and an average slope magnitude of about 2.54 degrees along the y-direction.

FIGS. 18A-18C are top-view scanning electron micrographs (SEMs) of a sample at three different magnifications. The sample was made using a cutter similar to cutter 1120 where the apex angle of the cutting tip 1125 was about 176 degrees. The sample was geometrically symmetric. Using confocal microscopy, the average height of the microstructures was measured to be about 2.67 microns. FIGS. 19A-19C are top-view SEMs of a sample at three different magnifications. The sample was made using a cutter similar to cutter 1110 where the radius of the cutting tip 1115 was about 480 microns. The sample was geometrically symmetric. Using confocal microscopy, the average height of the microstructures was measured to be about 2.56 microns. FIGS. 20A-20C are top-view SEMs of a sample at three different magnifications. The sample was made using a cutter similar to cutter 1110 where the radius of the cutting tip 1115 was about 3300 microns. The sample was geometrically asymmetric. Using confocal microscopy, the average height of the microstructures was measured to be about 1.46 microns.

The surfaces of a number of samples fabricated using the process outlined above were characterized over an area of about 200 microns by about 200 microns using atomic force microscopy (AFM). FIG. 21 is an exemplary AFM surface profile of one such sample, labeled sample A. The sample had an optical transmission of about 94.9%, an optical haze of about 1.73%, and an optical clarity of about 79.5%. FIGS. 22A and 22B are exemplary cross-sectional profiles of sample A along the x- and y-directions, respectively. FIG. 23 shows the percent slope distribution along the x- and y-directions for sample A. Slopes S_x and S_y along respective x- and y-directions were calculated from the following two expressions:

$$S_x = \partial H(x,y) / \partial x \quad (1)$$

$$S_y = \partial H(x,y) / \partial y \quad (2)$$

where $H(x,y)$ is the surface profile. The slopes S_x and S_y were calculated using a slope bin size of 0.5 degrees. As is evident from FIG. 23, sample A had a symmetric slope distribution along both the x- and the y-directions. Sample A had a broader slope distribution along the x-direction and a narrower slope distribution along the y-direction. FIG. 24 shows the percent height distribution across the analyzed surface for sample A. As is evident from FIG. 24, the sample had a substantially symmetric height distribution relative to the

12

peak height of the sample which was about 4.7 microns. FIG. 25 shows the percent slope magnitude for sample A, where the slope magnitude S_m was calculated from the following expression:

$$S_m = \sqrt{[\partial H / \partial x]^2 + [\partial H / \partial y]^2} \quad (3)$$

FIG. 26 shows the percent cumulative slope distribution $S_c(\theta)$ for sample A, where $S_c(\theta)$ was calculated from the following expression:

$$S_c(\theta) = \frac{\int_0^\theta S_m}{\int_0^\infty S_m} \quad (4)$$

As is evident from FIG. 26, about 100% of the surface of sample A had a slope magnitude less than about 3.5 degrees. Furthermore, about 52% of the analyzed surface had slope magnitudes less than about 1 degree, and about 72% of the analyzed surface had slope magnitudes less than about 1.5 degrees.

Three additional samples similar to sample A, and labeled B, C, and D, were characterized as previously outlined. All four samples A-D had microstructures similar to microstructures 160 and were made using a cutting tool system similar to cutting tool system 1000 to make a patterned roll using a cutter similar to cutter 1120 and subsequently microreplicating the patterned tool to make matte layers similar to matter layer 140. Sample B had an optical transmittance of about 95.2%, an optical haze of about 3.28% and an optical clarity of about 78%; Sample C had an optical transmittance of about 94.9%, an optical haze of about 2.12%, and an optical clarity of about 86.1%; and sample D had an optical transmittance of about 94.6%, an optical haze of about 1.71%, and an optical clarity of about 84.8%. In addition, six comparative samples, labeled R1-R6, were characterized. Samples R1-R3 were similar to matte layer 860 and included a plurality of large beads dispersed in a binder, where the matte surfaces were primarily formed because of the beads. Sample R1 had an optical haze of about 17.8% and an optical clarity of about 48.5%, sample R2 (available from Dai Nippon Printing Co., Ltd.) had an optical haze of about 32.2% and an optical clarity of about 67.2%, and sample R3 had an optical haze of about 4.7% and an optical clarity of about 73.3%. Sample R4 was an embossed polycarbonate film (available from Keiwa Inc., Osaka, Japan) and had an optical haze of about 23.2% and an optical clarity of about 39.5%.

FIG. 27 is the percent cumulative slope distribution $S_c(\theta)$ for samples A-D and R1-R4. Each of samples A-D was similar to matte layer 140 and included a structured major surface similar to structured major surface 120. As evident from FIG. 27, no more than about 7%, or about 6.5%, or about 6%, or about 5.5%, or about 5%, or about 4.5%, or about 4%, or about 3.5%, or about 3%, of the structured major surfaces of all, or at least some, of the samples A-D had a slope magnitude greater than about 3.5 degrees. Furthermore, no more than about 4%, or about 3.5%, or about 3%, or about 2.5%, or about 2%, or about 1.5%, or about 1%, or about 0.9%, or about 0.8%, of the structured major surfaces of all, or at least some, of the samples A-D had a cumulative slope magnitude greater than about 5 degrees.

Referring back to FIG. 1, when used in an optical system such as in a liquid crystal display, light redirecting film 100 is capable of hiding or masking optical and/or physical defects of the display and enhancing the brightness of the display. In some cases, the average effective transmission of light redi-

recting film **100** is less by no more than about 2%, or by no more than about 1.5%, or by no more than about 1%, or by no more than about 0.75%, or by no more than about 0.5%, as compared to a light redirecting film that has the same construction as light redirecting film **100**, except for having a smooth second major surface **120**. In some cases, the average effective transmission of the light redirecting film is greater than by no less than about 0.2%, or about 0.3%, or about 0.4%, or about 0.5%, or about 1%, or about 1.5%, or about 2%, as compared to a light redirecting film that has the same construction, except for having a smooth second major surface. As an example, a light redirecting film was fabricated that was similar to light redirecting film **100**. Linear prisms **150** had a pitch of about 24 microns, an apex angle **152** of about 90 degrees, and index of refraction of about 1.65. Second major surface **120** had an optical haze of about 1.5% and an optical clarity of about 83%. The light redirecting film had an average effective transmission of about 1.803. For comparison, a similar light redirecting film that had the same construction (including material composition) except for comprising a smooth second major surface, had an average effective transmission of about 1.813.

As another example, a light redirecting film was fabricated that was similar to light redirecting film **100**. Microstructures **160** were made by replication from a tool that was cut with a cutter similar to cutter **1110** where the radius of cutter tip **1115** was about 3300 microns. Linear prisms **150** had a pitch of about 24 microns, an apex angle **152** of about 90 degrees, and index of refraction of about 1.567. Second major surface **120** had an optical haze of about 1.71% and an optical clarity of about 84.8%. The light redirecting film had an average effective transmission of about 1.633. For comparison, a similar light redirecting film that had the same construction (including material composition) except for comprising a smooth second major surface, had an average effective transmission of about 1.626. Hence, the structured second major surface **120** provided additional gain by increasing the average effective transmission by about 0.43%.

As another example, a light redirecting film was fabricated that was similar to light redirecting film **100**. Microstructures **160** were made by replication from a tool that was cut with a cutter similar to cutter **1110** where the radius of cutter tip **1115** was about 4400 microns. Linear prisms **150** had a pitch of about 24 microns, an apex angle **152** of about 90 degrees, and index of refraction of about 1.567. Second major surface **120** had an optical haze of about 1.49% and an optical clarity of about 82.7%. The light redirecting film had an average effective transmission of about 1.583. For comparison, a similar light redirecting film that had the same construction (including material composition) except for comprising a smooth second major surface, had an average effective transmission of about 1.578. Hence, the structured second major surface **120** provided additional gain by increasing the average effective transmission by about 0.32%.

As yet another example, a light redirecting film was fabricated that was similar to light redirecting film **100**. Microstructures **160** were made by replication from a tool that was cut with a cutter similar to cutter **1110** where the radius of cutter tip **1115** was about 3300 microns. Linear prisms **150** had a pitch of about 24 microns, an apex angle **152** of about 90 degrees, and index of refraction of about 1.567. Second major surface **120** had an optical haze of about 1.35% and an optical clarity of about 85.7%. The light redirecting film had an average effective transmission of about 1.631. For comparison, a similar light redirecting film that had the same construction (including material composition) except for comprising a smooth second major surface, had an average

effective transmission of about 1.593. Hence, the structured second major surface **120** provided additional gain by increasing the average effective transmission by about 2.38%.

Substrate layer **170** can be or include any material that may be suitable in an application, such as a dielectric, a semiconductor, or a metal. For example, substrate layer **170** can include or be made of glass and polymers such as polyethylene terephthalate (PET), polycarbonates, and acrylics. Substrate **170** can be rigid or flexible. Substrate **170** can have any thickness and/or index of refraction that may be desirable in an application. For example, in some cases, substrate layer **170** can be PET and have a thickness of about 50 microns or about 175 microns.

FIG. **28** is a schematic side-view of an optical stack **2800** that includes a first light redirecting film **2805** disposed on a second light redirecting film **2855**. One or both of the light redirecting films can be similar to light redirecting film **100**. First light redirecting film **2805** includes a first major surface **2810** and an opposing second major surface **2815**. The first major surface includes a first plurality of microstructures **2820** that extend along the y-direction, and the second major surface includes a second plurality of microstructures **2825**. Second light redirecting film **2855** includes a third major surface **2860** and an opposing fourth major surface **2865**. Third major surface **2860** faces second major surface **2815** of the first light redirecting film and includes a third plurality of microstructures **2870** that extend along a different direction than the y-direction, such as the x-direction. Fourth major surface **2865** includes a fourth plurality of microstructures **2875**.

In some cases, first light redirecting film **2805** includes a matte layer **2880** that includes second major surface **2815**. Similarly, in some cases, second light redirecting film **2855** includes a matte layer **2885** that includes fourth major surface **2865**.

In some cases, such as when optical stack **2800** is included in the backlight of a liquid crystal display, linear microstructures **2820** and/or **2870** can give rise to moiré. In some cases, the two light redirecting films, and in particular, the top light redirecting film, can give rise to color mura. Color mura is due to the index dispersion of the light redirecting films. The first order color mura is typically visible close to the viewing angle limit of the light redirecting film while higher order color mura are typically visible at higher angles. In some cases, such as when major surfaces **2815** and **2865** have sufficiently low optical haze and clarity, the optical stack can effectively mask or eliminate moiré and color mura without significantly reducing the display brightness. In such cases, each of the second and fourth major surfaces has an optical haze that is not greater than about 5%, or not greater than about 4.5%, or not greater than about 4%, or not greater than about 3.5%, or not greater than about 3%, or not greater than about 2.5%, or not greater than about 2%, or not greater than about 1.5%, or not greater than about 1%; and each of the second and fourth major surfaces has an optical clarity that is not greater than about 85%, or not greater than about 80%, or not greater than about 75%, or not greater than about 70%, or not greater than about 65%, or not greater than about 60%.

In some cases, such as when optical stack **2800** is used in a display system to increase the brightness, the average effective transmission (ETA) of the optical stack is not less than about 2.4, or not less than about 2.45, or not less than about 2.5, or not less than about 2.55, or not less than about 2.6, or not less than about 2.65, or not less than about 2.7, or not less than about 2.75, or not less than about 2.8. In some cases, the average effective transmission of optical stack **2800** is less by no more than about 1%, or about 0.75%, or about 0.5%, or

15

about 0.25%, or about 0.1%, as compared to an optical stack that has the same construction (including material composition) except for comprising smooth second and fourth major surfaces. In some cases, the average effective transmission of optical stack **2800** is not less as compared to an optical stack that has the same construction except for having smooth second and fourth major surfaces. In some cases, the average effective transmission of optical stack **2800** is greater by at least about 0.1%, or about 0.2%, or about 0.3%, as compared to an optical stack that has the same construction except for comprising smooth second and fourth major surfaces. As an example, an optical stack was fabricated that was similar to optical stack **2800** and had an average effective transmission of about 2.773. Each of respective second and fourth major surfaces **2815** and **2865** had an optical haze of about 1.5% and an optical clarity of about 83%. The linear prisms had an index of refraction of about 1.65. For comparison, a similar optical stack that had the same construction except for including smooth second and fourth major surfaces, had an average effective transmission of about 2.763. Hence, the structured bottom major surfaces **2815** and **2865** provided additional again by increasing the average effective transmission by about 0.36%.

As another example, an optical stack was fabricated that was similar to optical stack **2800** and had an average effective transmission of about 2.556. Each of respective second and fourth major surfaces **2815** and **2865** had an optical haze of about 1.29% and an optical clarity of about 86.4%. The linear prisms had a pitch of about 24 microns, an apex angle of about 90 degrees, and an index of refraction of about 1.567. For comparison, a similar optical stack that had the same construction except for including smooth second and fourth major surfaces, had an average effective transmission of about 2.552. Hence, the structured bottom major surfaces **2815** and **2865** provided additional again by increasing the average effective transmission by about 0.16%.

As yet another example, an optical stack was fabricated that was similar to optical stack **2800** and had an average effective transmission of about 2.415. Each of respective second and fourth major surfaces **2815** and **2865** had an optical haze of about 1.32% and an optical clarity of about 84.8%. The linear prisms had a pitch of about 24 microns, an apex angle of about 90 degrees, and an index of refraction of about 1.567. For comparison, a similar optical stack that had the same construction except for including smooth second and fourth major surfaces, had an average effective transmission of about 2.404. Hence, the structured bottom major surfaces **2815** and **2865** provided additional again by increasing the average effective transmission by about 0.46%.

FIG. **29** is a schematic side-view of a display system **2900** for displaying information to a viewer **2999**. The display system includes a liquid crystal panel **2910** that is disposed on and is illuminated by a backlight **2920**. Liquid crystal panel **2910** includes a liquid crystal cell **2930** that is disposed between linear light absorbing polarizers **2935** and **2940**. In some cases, such as when display system **2900** displays an image to viewer **2999**, liquid crystal panel **2910** can be pixelated.

Backlight **2920** includes a lightguide **2970** that receives light through an edge of the lightguide from a lamp **2990** that is housed in a side reflector **2995**, a back reflector **2980** for reflecting light that is incident on the back reflector toward viewer **2999**, an optical diffuser **2960** for homogenizing light **2985** that exits from an emitting surface **2975** of the lightguide, and optical stack **2800** from FIG. **28** disposed between the optical diffuser and a reflective polarizer **2950**.

16

Optical stack **2800** includes light redirecting films **2805** and **2855**. In some cases, linear prisms of the two light redirecting films are orthogonally oriented relative to each other. For example, linear prisms **2820** can extend along the y-direction and linear prisms **2870** can be oriented along the x-direction. Microstructures **2825** and **2875** face lightguide **2970** and prismatic microstructures **2820** and **2870** face away from the lightguide.

Optical stack **2800** enhances the brightness, such as the on-axis brightness, of the display system. At the same time, respective second and fourth major surfaces **2815** and **2865** of the optical stack have sufficiently low optical clarities to mask physical defects such as scratches, and hide and/or eliminate optical defects such moiré and color mora.

Reflective polarizer **2950** substantially reflects light that has a first polarization state and substantially transmits light that has a second polarization state, where the two polarization states are mutually orthogonal. For example, the average reflectance of reflective polarizer **2950** in the visible for the polarization state that is substantially reflected by the reflective polarizer is at least about 50%, or at least about 60%, or at least about 70%, or at least about 80%, or at least about 90%, or at least about 95%. As another example, the average transmittance of reflective polarizer **2950** in the visible for the polarization state that is substantially transmitted by the reflective polarizer is at least about 50%, or at least about 60%, or at least about 70%, or at least about 80%, or at least about 90%, or at least about 95%, or at least about 97%, or at least about 98%, or at least about 99%. In some cases, reflective polarizer **2950** substantially reflects light having a first linear polarization state (for example, along the x-direction) and substantially transmits light having a second linear polarization state (for example, along the y-direction).

Any suitable type of reflective polarizer may be used for reflective polarizer layer **2950** such as, for example, a multi-layer optical film (MOF) reflective polarizer, a diffusely reflective polarizing film (DRPF) having a continuous phase and a disperse phase, such as a Vikuiti™ Diffuse Reflective Polarizer Film ("DRPF") available from 3M Company, St. Paul, Minn., a wire grid reflective polarizer described in, for example, U.S. Pat. No. 6,719,426, or a cholesteric reflective polarizer.

For example, in some cases, reflective polarizer **2950** can be or include an MOF reflective polarizer, formed of alternating layers of different polymer materials, where one of the sets of alternating layers is formed of a birefringent material, where the refractive indices of the different materials are matched for light polarized in one linear polarization state and unmatched for light in the orthogonal linear polarization state. In such cases, an incident light in the matched polarization state is substantially transmitted through reflective polarizer **2950** and an incident light in the unmatched polarization state is substantially reflected by reflective polarizer **2950**. In some cases, an MOF reflective polarizer **2950** can include a stack of inorganic dielectric layers.

As another example, reflective polarizer **2950** can be or include a partially reflecting layer that has an intermediate on-axis average reflectance in the pass state. For example, the partially reflecting layer can have an on-axis average reflectance of at least about 90% for visible light polarized in a first plane, such as the xy-plane, and an on-axis average reflectance in a range from about 25% to about 90% for visible light polarized in a second plane, such as the xz-plane, perpendicular to the first plane. Such partially reflecting layers are described in, for example, U.S. Patent Publication No. 2008/064133, the disclosure of which is incorporated herein in its entirety by reference.

In some cases, reflective polarizer **2950** can be or include a circular reflective polarizer, where light circularly polarized in one sense, which may be the clockwise or counterclockwise sense (also referred to as right or left circular polarization), is preferentially transmitted and light polarized in the opposite sense is preferentially reflected. One type of circular polarizer includes a cholesteric liquid crystal polarizer.

In some cases, reflective polarizer **2950** can be a multilayer optical film that reflects or transmits light by optical interference, such as those described in Provisional U.S. Patent Application No. 61/116,132, filed Nov. 19, 2009; Provisional U.S. Patent Application No. 61/116,291, filed Nov. 19, 2008; Provisional U.S. Patent Application No. 61/116,294, filed Nov. 19, 2008; Provisional U.S. Patent Application No. 61/116,295, filed Nov. 19, 2008; Provisional U.S. Patent Application No. 61/116,295, filed Nov. 19, 2008; and International Patent Application No. PCT/US 2008/060311, filed May 19, 2008, claiming priority from Provisional U.S. Patent Application No. 60/939,085, filed Apr. 15, 2000; all incorporated herein by reference in their entirety.

Optical diffuser **2960** has the primary functions of hiding or masking lamp **2990** and homogenizing light **2985** that is emitted by lightguide **2970**. Optical diffuser **2960** has a high optical haze and/or a high diffuse optical reflectance. For example, in some cases, the optical haze of the optical diffuser is not less than about 40%, or not less than about 50%, or not less than about 60%, or not less than about 70%, or not less than about 80%, or not less than about 85%, or not less than about 90%, or not less than about 95%. As another example, the diffuse optical reflectance of the optical diffuser is not less than about 30%, or not less than about 40%, or not less than about 50%, or not less than about 60%.

Optical diffuser **2960** can be or include any optical diffuser that may be desirable and/or available in an application. For example, optical diffuser **2960** can be or include a surface diffuser, a volume diffuser, or a combination thereof. For example, optical diffuser **2960** can include a plurality of particles having a first index of refraction n_1 dispersed in a binder or host medium having a different index of refraction n_2 , where the difference between the two indices of refraction is at least about 0.01, or at least about 0.02, or at least about 0.03, or at least about 0.04, or at least about 0.05.

Back reflector **2980** receives light that is emitted by the lightguide away from viewer **2999** along the negative z-direction and reflects the received light towards the viewer. Display systems such as display system **2900** where lamp **2990** is placed along an edge of a lightguide, are generally referred to as edge-lit or backlit displays or optical systems. In some cases, the back reflector can be partially reflective and partially transmissive. In some cases, the back reflector can be structured, for example, have a structured surface.

Back reflector **2980** can be any type reflector that may be desirable and/or practical in an application. For example, the back reflector can be a specular reflector, a semi-specular or

semi-diffuse reflector, or a diffuse reflector, such as those disclosed in International Patent Application No. PCT/US 2008/064115, filed May 19, 2008, claiming priority from Provisional U.S. Patent Application No. 60/939,085, filed May 20, 2007, both incorporated herein by reference in their entirety. For example, the reflector can be an aluminized film or a multi-layer polymeric reflective film, such as an enhanced specular reflector (ESR) film (available from 3M Company, St. Paul, Minn.). As another example, back reflector **2980** can be a diffuse reflector having a white appearance.

As used herein, terms such as “vertical”, “horizontal”, “above”, “below”, “left”, “right”, “upper” and “lower”, “clockwise” and “counter clockwise” and other similar terms, refer to relative positions as shown in the figures. In general, a physical embodiment can have a different orientation, and in that case, the terms are intended to refer to relative positions modified to the actual orientation of the device. For example, even if the image in FIG. 1 is flipped as compared to the orientation in the figure, first major surface **110** is still considered to be the top major surface.

All patents, patent applications, and other publications cited above are incorporated by reference into this document as if reproduced in full. While specific examples of the invention are described in detail above to facilitate explanation of various aspects of the invention, it should be understood that the intention is not to limit the invention to the specifics of the examples. Rather, the intention is to cover all modifications, embodiments, and alternatives falling within the spirit and scope of the invention as defined by the appended claims.

What is claimed is:

1. An optical film comprising a structured major surface comprising geometrical symmetry and asymmetric slope distribution, wherein no more than about 7% of the structured major surface has a slope magnitude greater than about 3.5 degrees or no more than about 4% of the structured major surface has a slope magnitude greater than about 5 degrees.
2. An optical film comprising a structured major surface comprising geometrical symmetry and asymmetric slope distribution, the optical film having an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%.
3. An optical film comprising a structured major surface comprising geometrical asymmetry and symmetric slope distribution, wherein no more than about 7% of the structured major surface has a slope magnitude greater than about 3.5 degrees or no more than about 4% of the structured major surface has a slope magnitude greater than about 5 degrees.
4. An optical film comprising a structured major surface comprising geometrical asymmetry and symmetric slope distribution, the optical film having an optical haze that is not greater than about 3% and an optical clarity that is not greater than about 85%.

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UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 9,229,239 B2
APPLICATION NO. : 14/186363
DATED : January 5, 2016
INVENTOR(S) : Joseph Aronson

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Specification


Column 4

Line 21, Delete "mora." and insert -- mura. --, therefor.

Column 16

Line 14, Delete "mora." and insert -- mura. --, therefor.

Signed and Sealed this
Eleventh Day of October, 2016

A handwritten signature in black ink, reading "Michelle K. Lee". The signature is fluid and cursive, with the first letters of each name being capitalized and prominent.

Michelle K. Lee
Director of the United States Patent and Trademark Office